

Power System Seminar 1

A Day in the Life of the NCC & Managing Transmission System

Marie Hayden

Michael Kelly

Agenda

- Two Presentations
 - Marie Hayden: The component parts of the transmission system & how it is operated in theory
 - Michael Kelly: Real Life – The what and how of transmission system operation in the NCC
- A visit to the National Control Centre

NCC – What do they do?

LEFT HAND SIDE - TRANSMISSION



- Voltage Control
 - 410–370kV, 240–210kV, 120–105kV
- Monitoring MVA flow on power lines,
 - Redispatch generators
 - Sectionalise stations if necessary
- Remote Control Operations, live switching
- Contingency and Alarm Monitoring
- Transmission Outage Management
- Restoration of plant following disconnection

RIGHT HAND SIDE - GENERATION

49 Hz 50 Hz 51 Hz

Next Seminar

- will look at this side
- The NCC instructs the generators to maintain a balance
 - Gen Deficit, f ↓ Excess Gen, f ↑
 - Ensure enough plant for next peak
 - Hydro targets, Gas Indicative Schedule
 - Maintain Reserve + Shared with SONI
 - Wind/ Load Forecast - RCUC

The Theory Presentation

- Overview of the Transmission System
- Differences between the Distribution System and the Transmission System
- The component parts of the Transmission system
- Voltage Control Theory
- Power Flow Control Theory
- Theory of the Meshed Network and N-1 Security

The High Voltage Transmission System

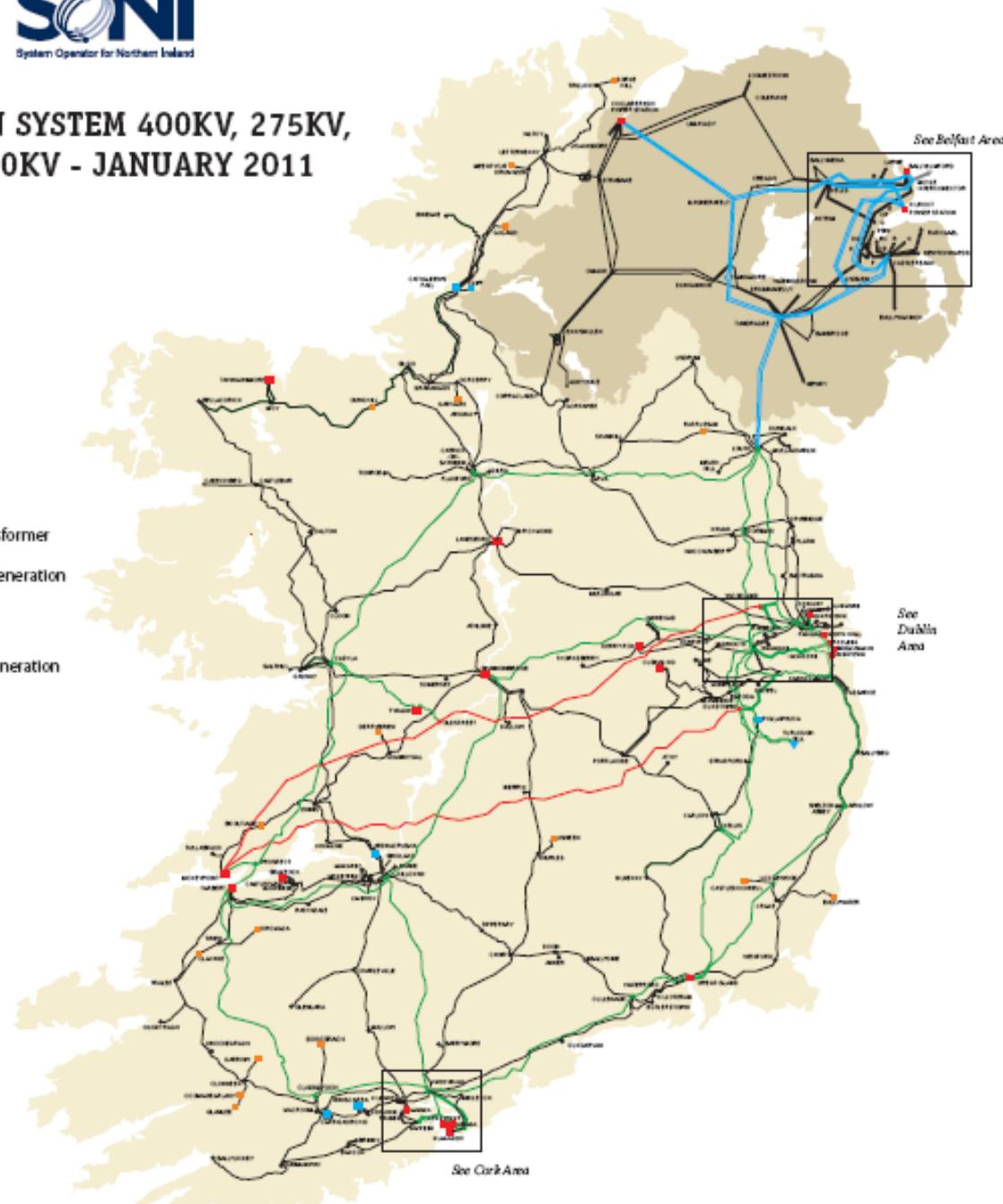
A transport network not unlike a road network





TRANSMISSION SYSTEM 400KV, 275KV, 220KV AND 110KV - JANUARY 2011

- 400kV Lines
- 275kV Lines
- 220kV Lines
- 110kV Lines
- 220kV Cables
- 110kV Cables
- 400kV Stations
- 275kV Stations
- 220kV Stations
- 110kV Stations
- Phase Shifting Transformer
- Transmission Connected Generation
 - Hydro Generation
 - Thermal Generation
 - ▼ Pumped Storage Generation
 - Wind Generation



Today you will see a few times the NCC
Schematic Representation of the
transmission system.

Let me talk through it briefly with you.

KV MW +KV MVAR +KV MVA +KV FREQ & DCC

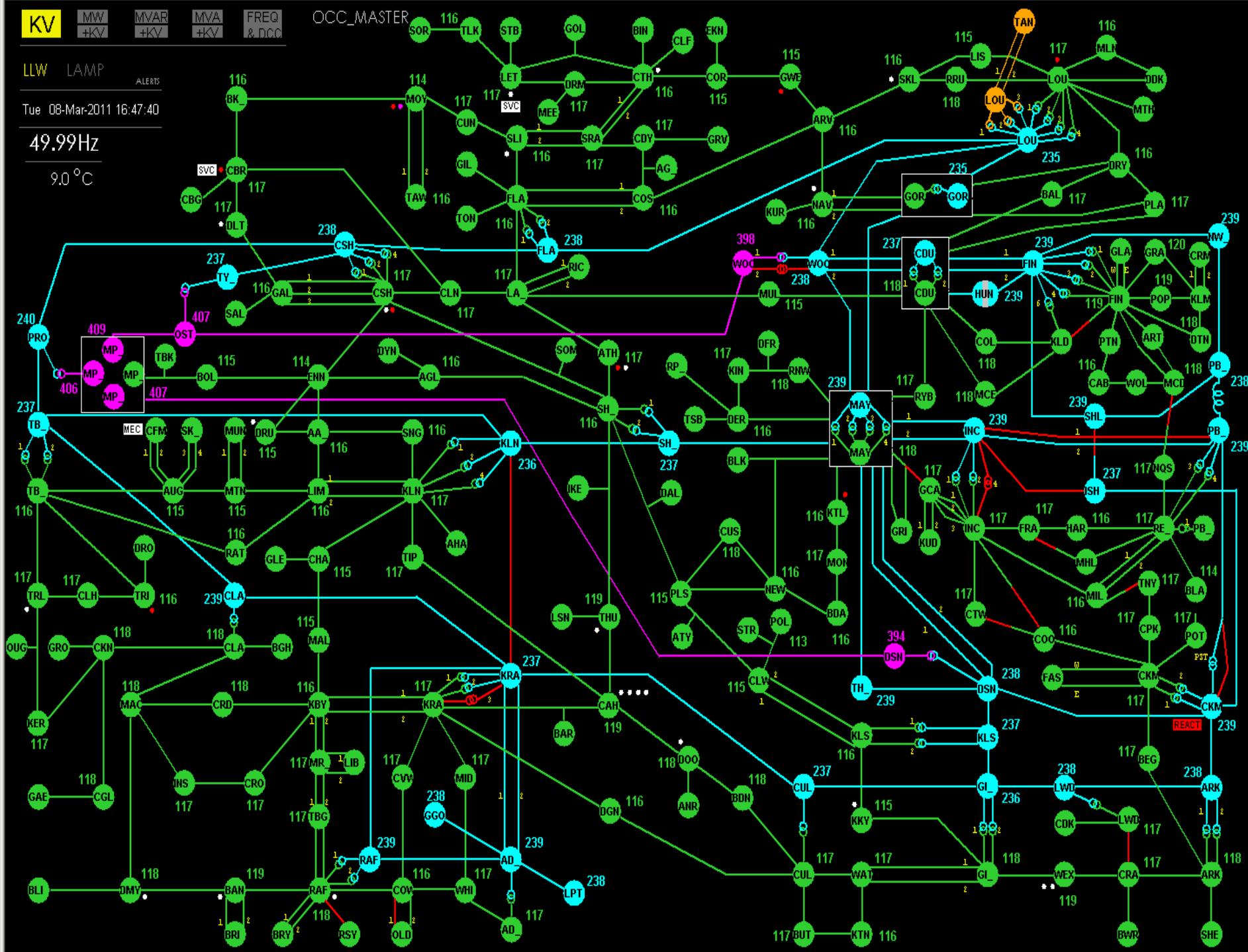
OCC_MASTER

LLW LAMP

Tue 08-Mar-2011 16:47:40

49.99Hz

9.0 °C



DISTRIBUTION V TRANSMISSION

Transmission Versus Distribution

- Principle Differences between Transmission and Distribution are:
 - Meshed V Radial Networks
 - When a transmission line trips power is re-routed to the station from other lines automatically without interruption
 - Example – Portlaoise had 4 lines feeding it
 - Size
 - More Customers are fed at each Transmission Station

KV MW +KV MVAR +KV MVA +KV FREQ & DCC

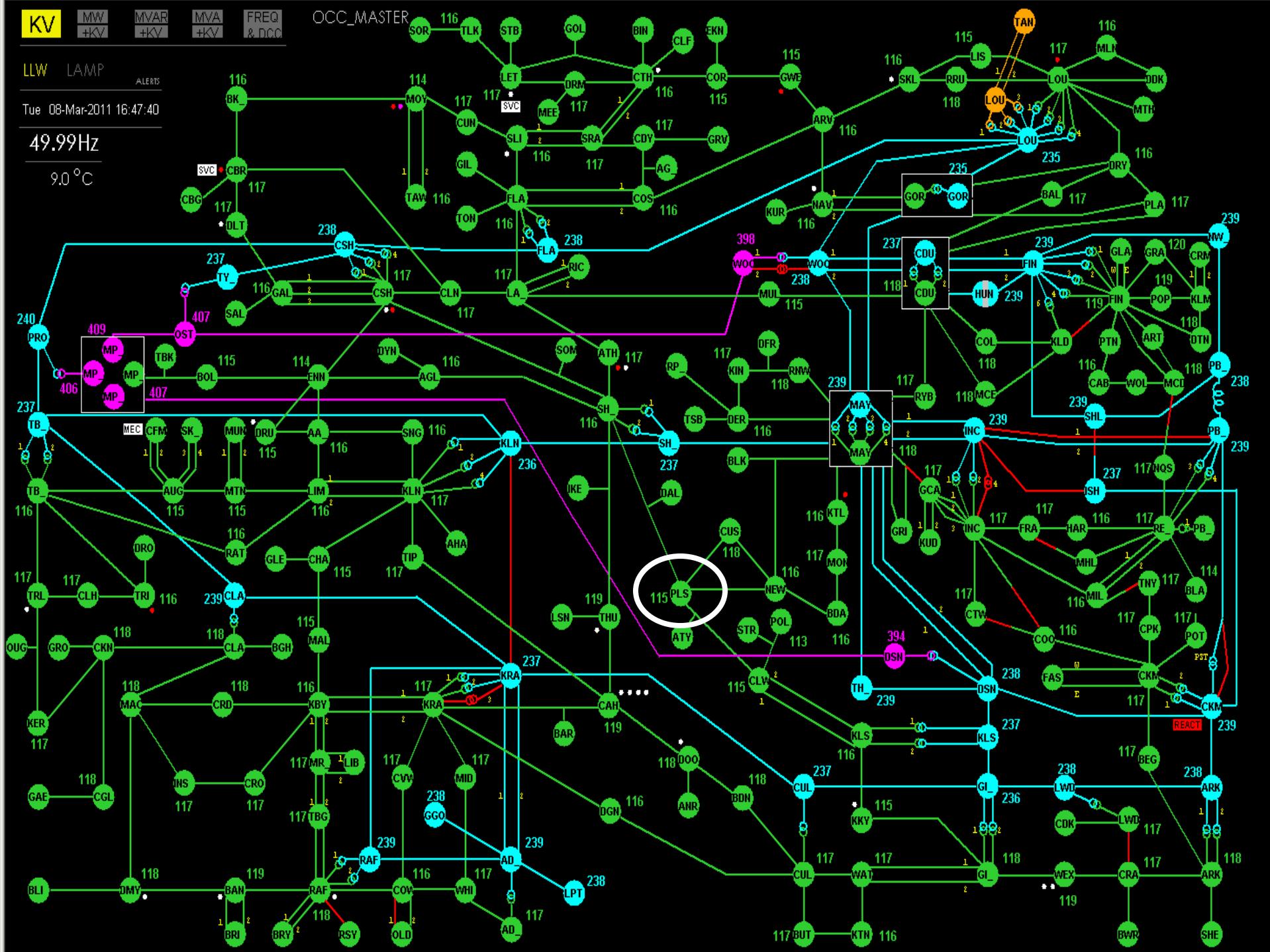
OCC_MASTER

LLW LAMP

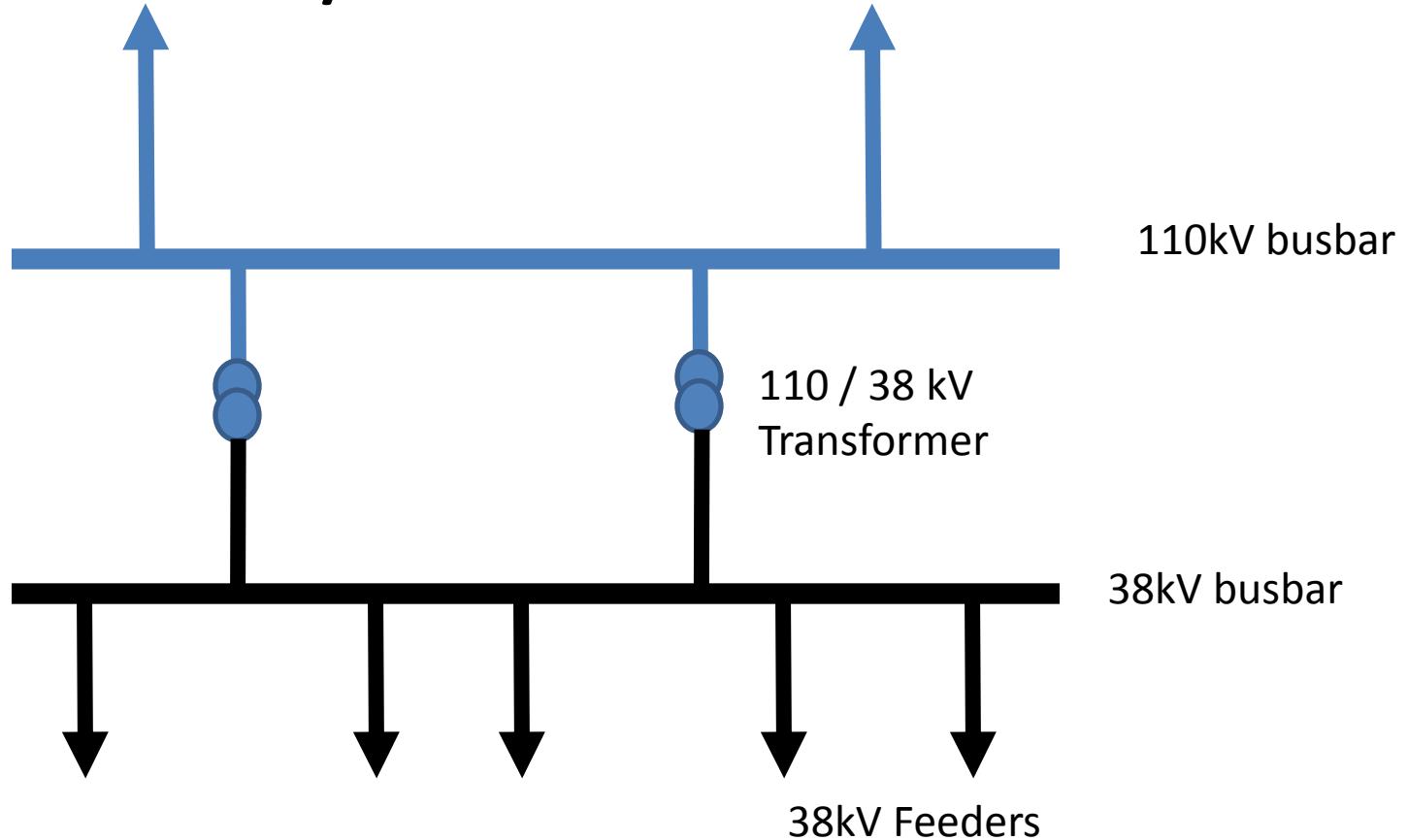
Tue 08-Mar-2011 16:47:40

49.99Hz

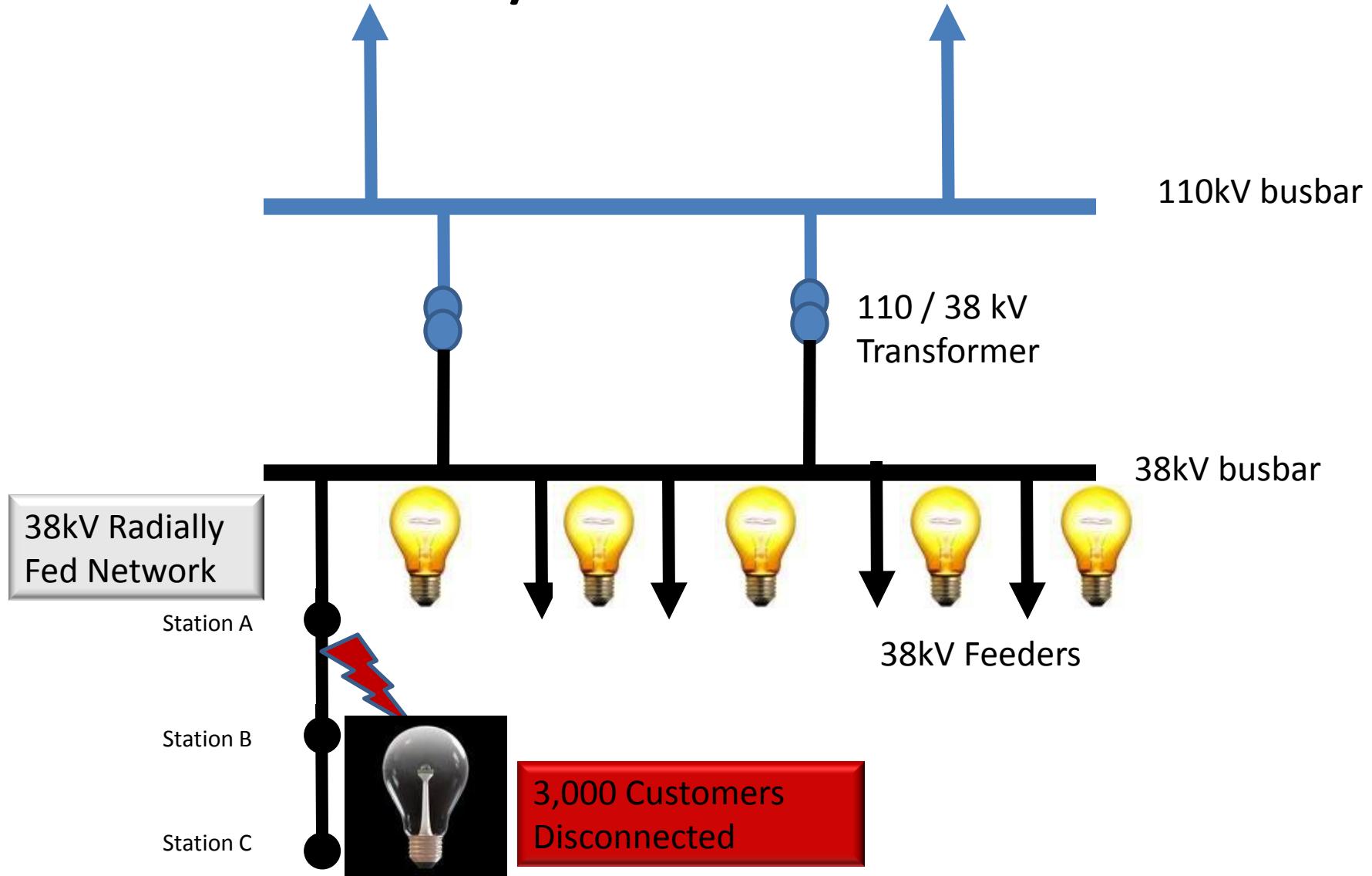
9.0 °C



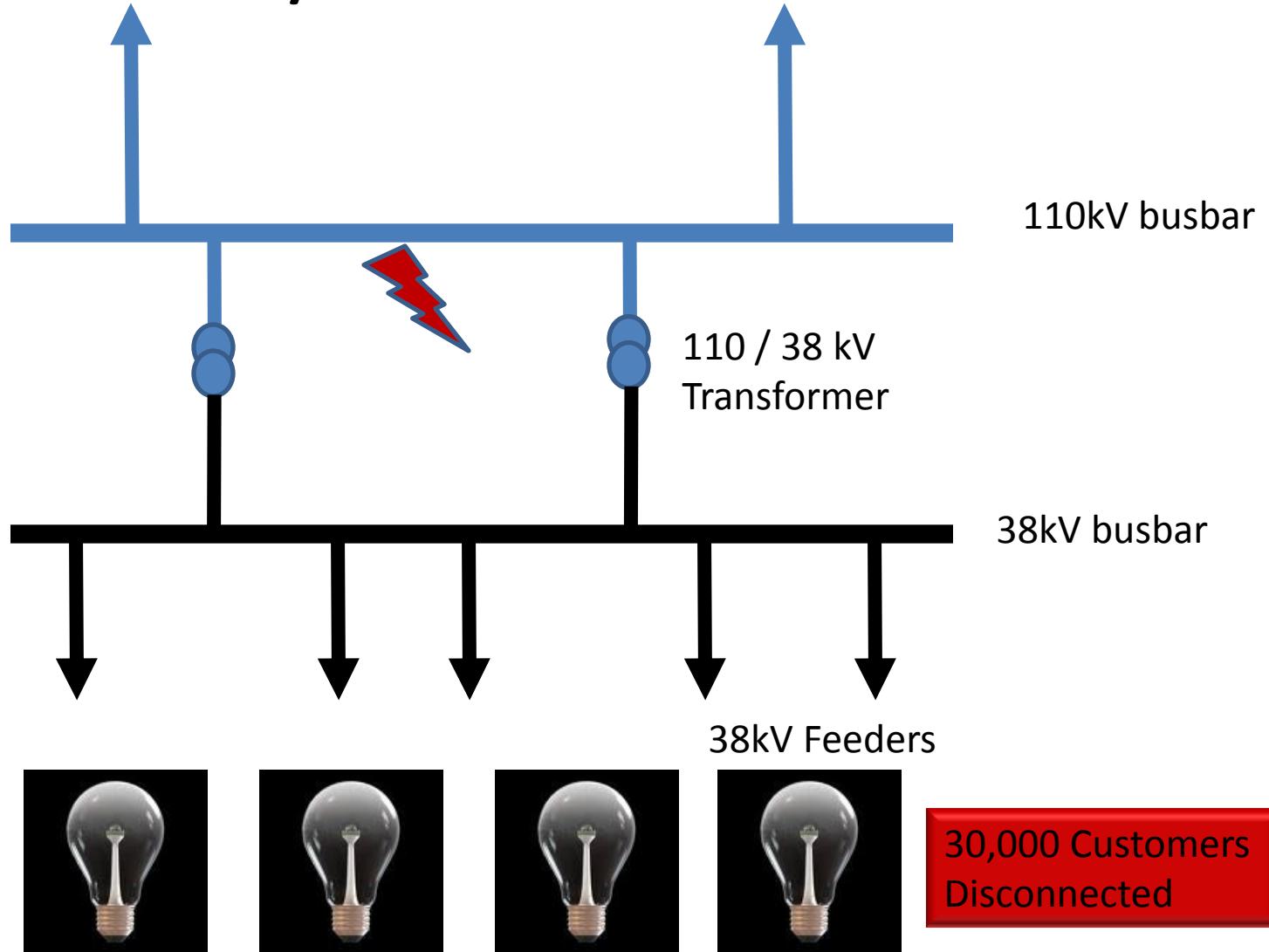
110 / 38kV Station



110 / 38kV Station



110 / 38kV Station



COMPONENT PARTS OF THE TRANSMISSION SYSTEM

Overhead Lines

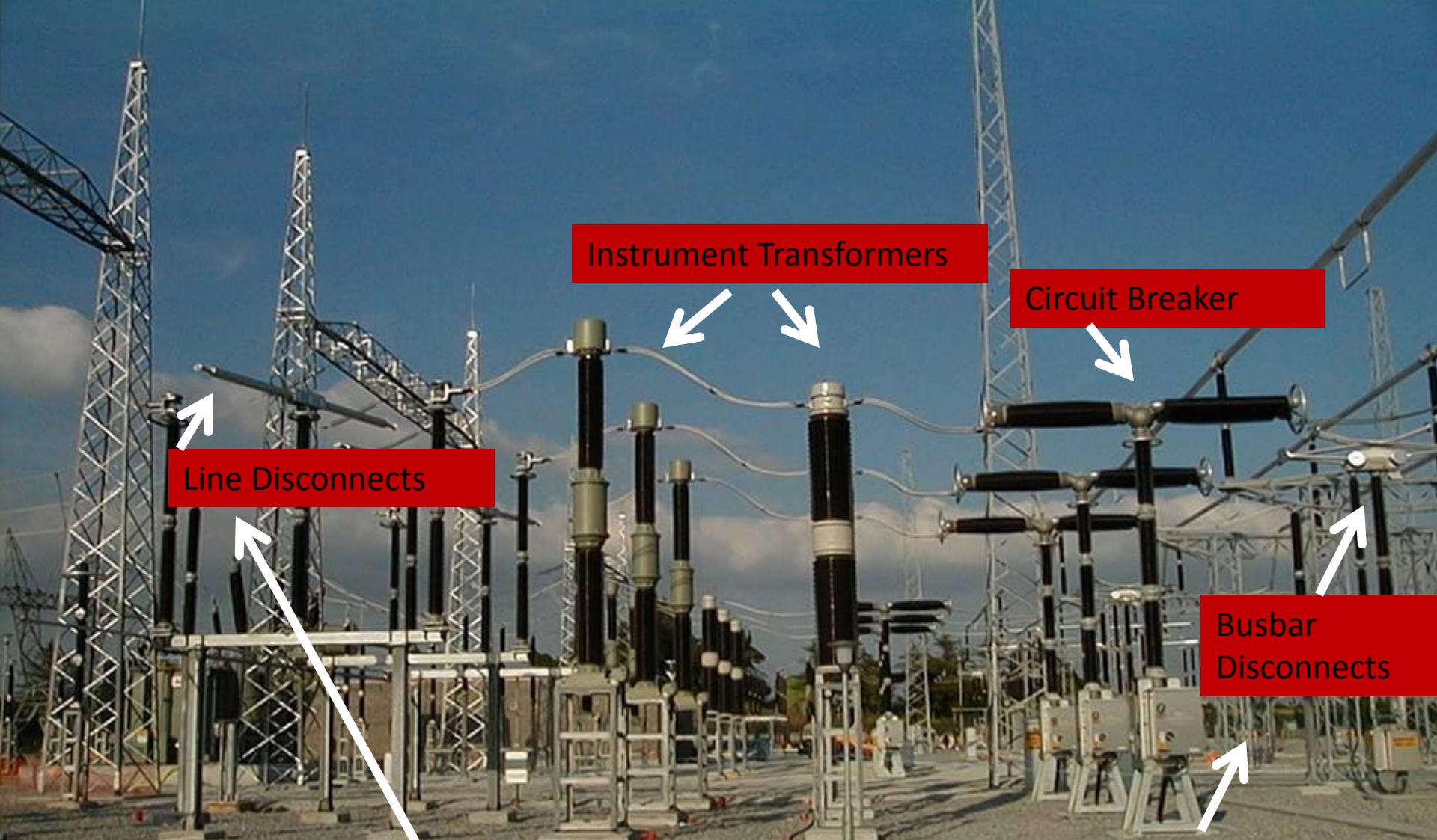


Underground Cables



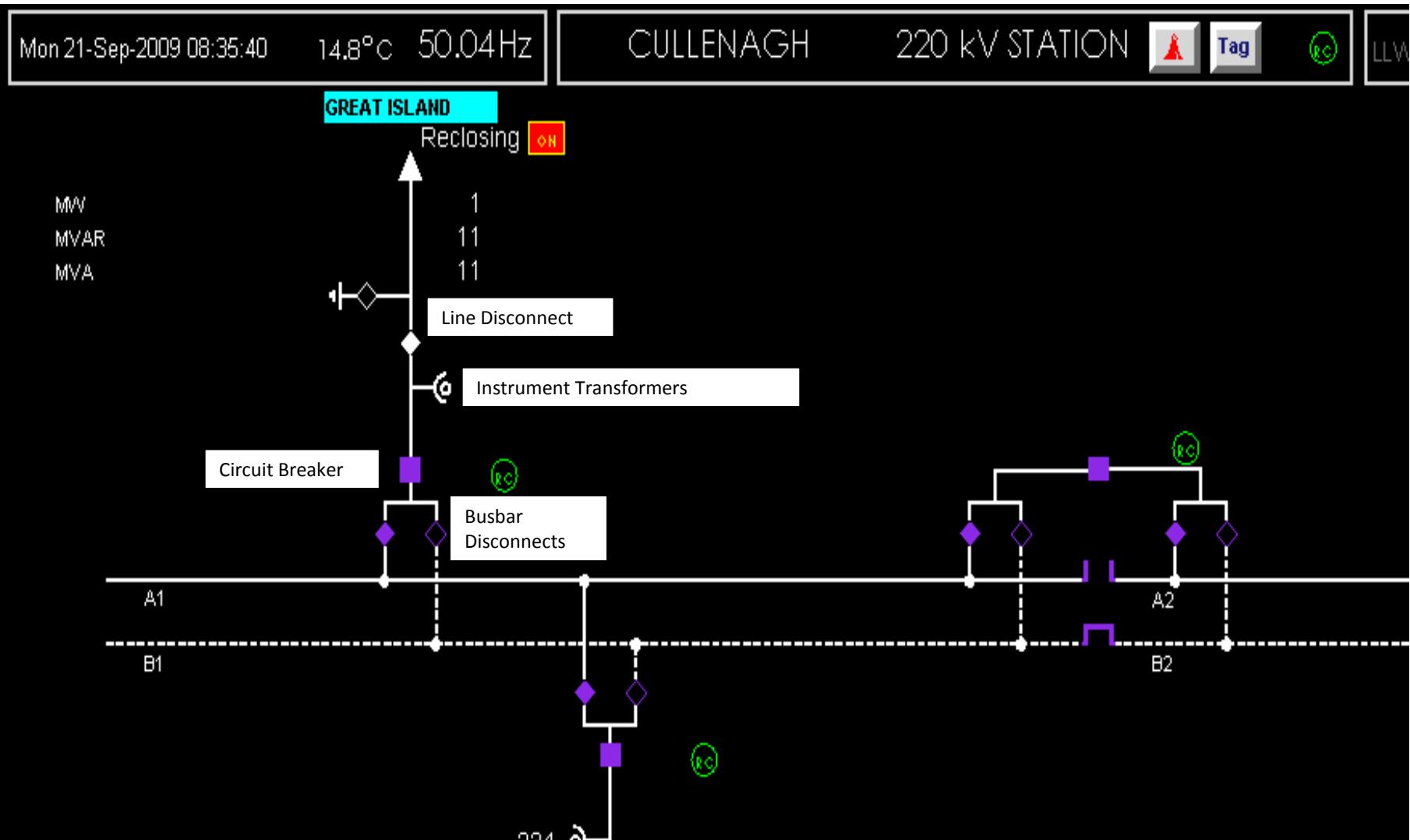
220kV Tubular Busbar with Pantograph Disconnects





NB Disconnects cannot Break Load Current
They provide points of isolation to allow work take place

In NCC all of this is represented as follows



Rating of Equipment

- As shown a Circuit is made up of
 - The Line or Cable
 - The circuit breaker
 - Disconnects
 - Instrument transformers
- Each of these has a rating above which it cannot be operated
- All of these items must be maintained
- A fault on any of these items will cause the circuit to trip and possibly more than just that circuit

THEORY OF VOLTAGE CONTROL

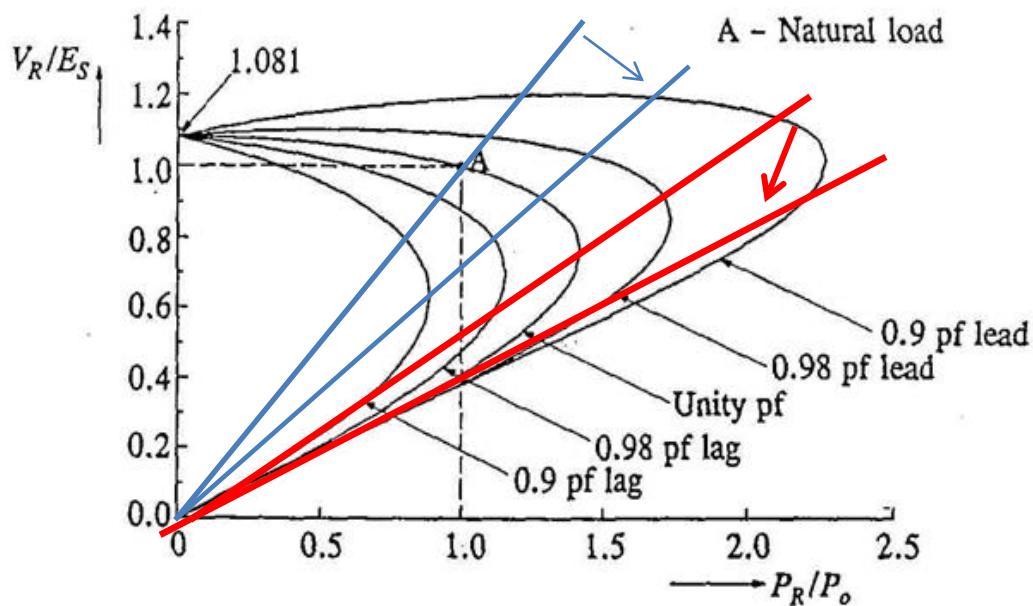
Voltage and Power Flow Control

- As demand for real power (MW) increases so does demand for reactive power
- If reactive power demand is not carefully managed over-voltages or under-voltages can occur
- Voltage Control is a steady state and a dynamic problem

Steady State

- Reactive Power can be supplied by
 - Generators
 - Capacitors / Reactors
 - Transmission Lines & Cables
- Controller must manage MVAR across the system to maintain voltages within allowable limits
- Not as easy as it sounds - much harder than MW control
- If NCC do not constantly manage voltage the voltage can collapse very rapidly

Voltage Collapse



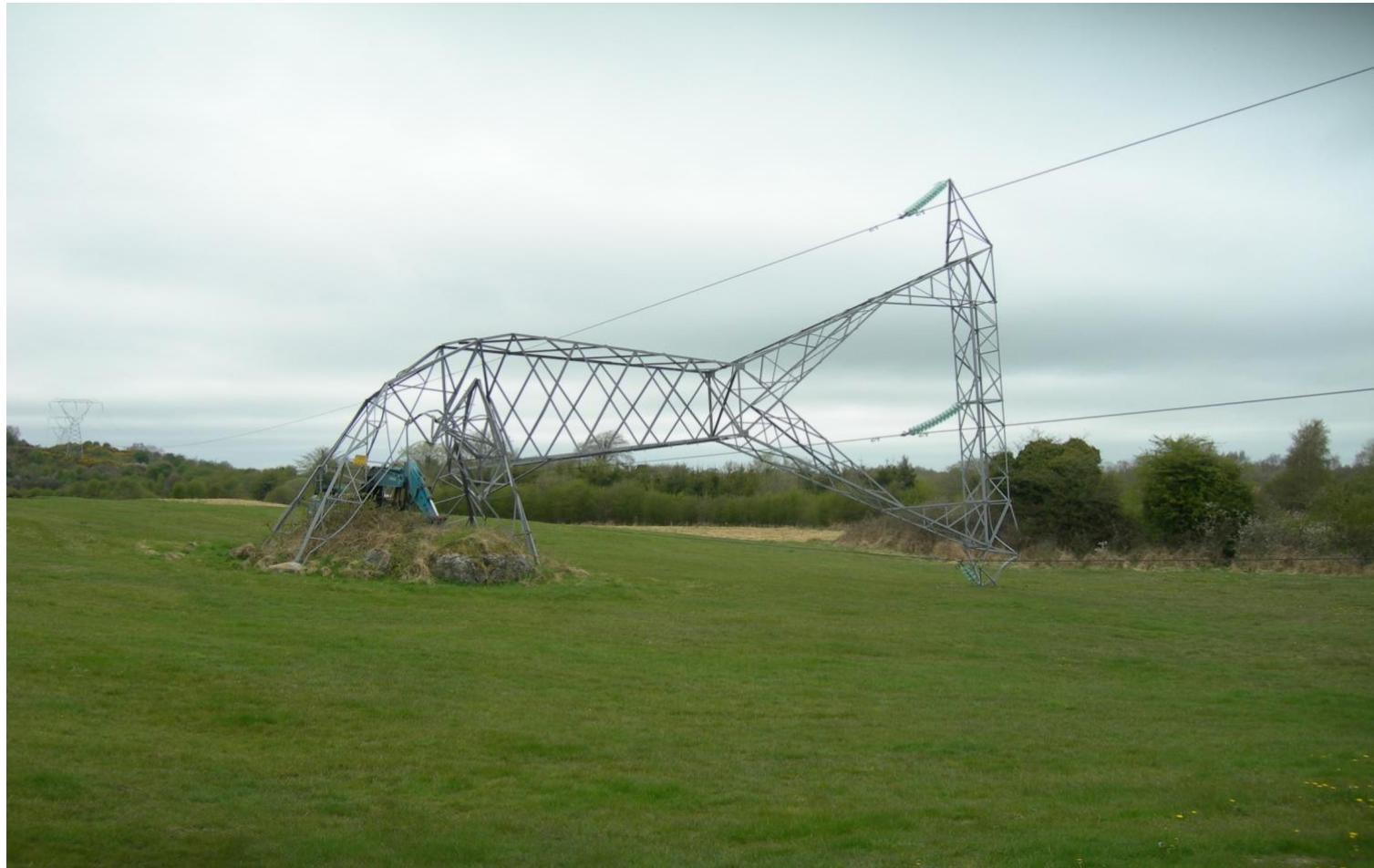
- Voltage Collapse can happen in a matter of minutes
- It has been the cause of wide-scale blackouts in other countries

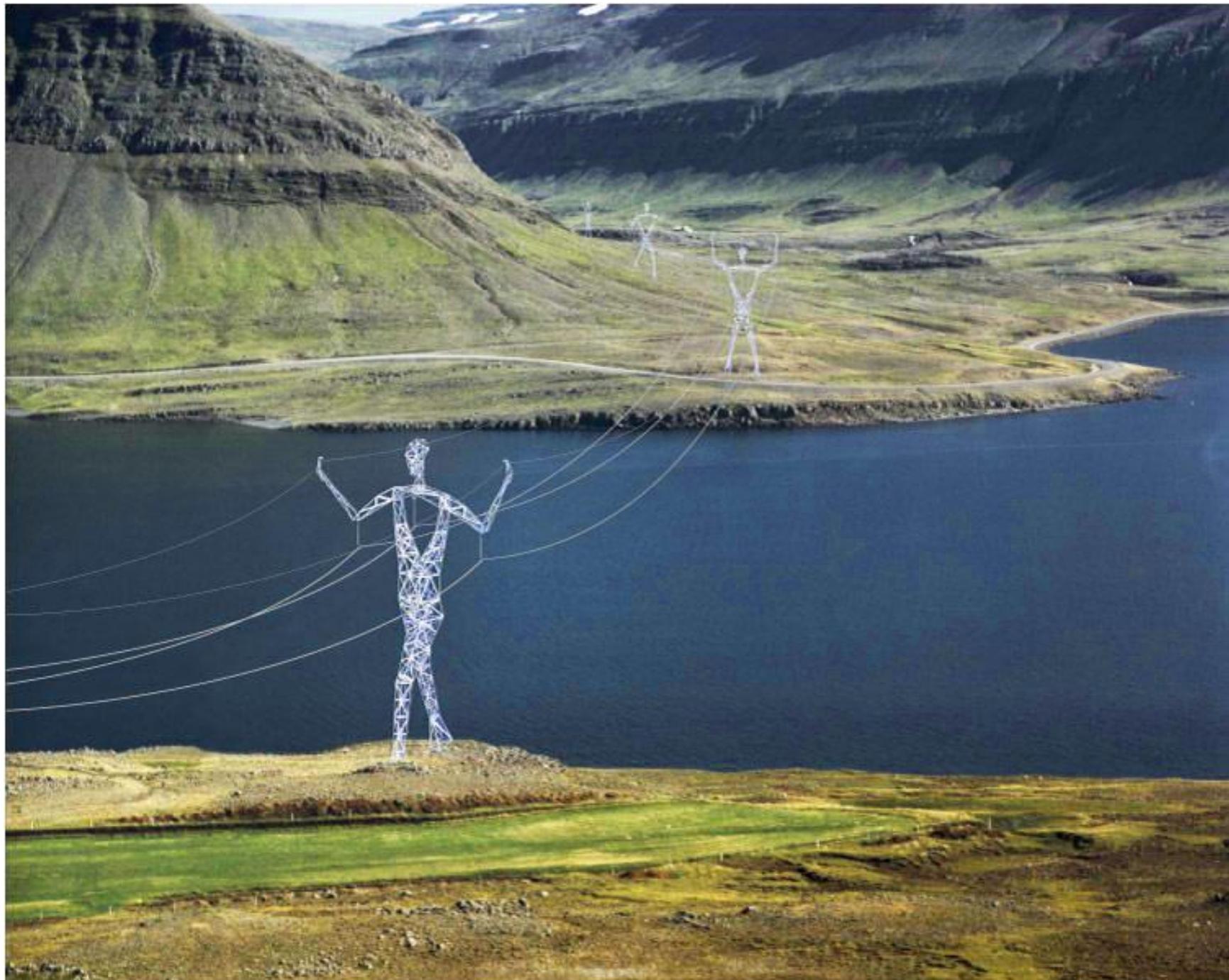
THEORY OF OVERLOAD CONTROL

Transmission Plant Ratings

- All items of plant are designed to operate at a specific temperature.
- For overhead power lines the actual conductor temperature is influenced by
 - the current flowing down the line and
 - ambient conditions such as wind, temperature, sunlight.
- Static Ratings reflect the allowable power flow for a given ambient conditions
- EirGrid is trialling Dynamic Line Rating Equipment at the moment
- Power lines carrying too much current will sag and could come into contact with earth.

This is not what I mean by sag!!



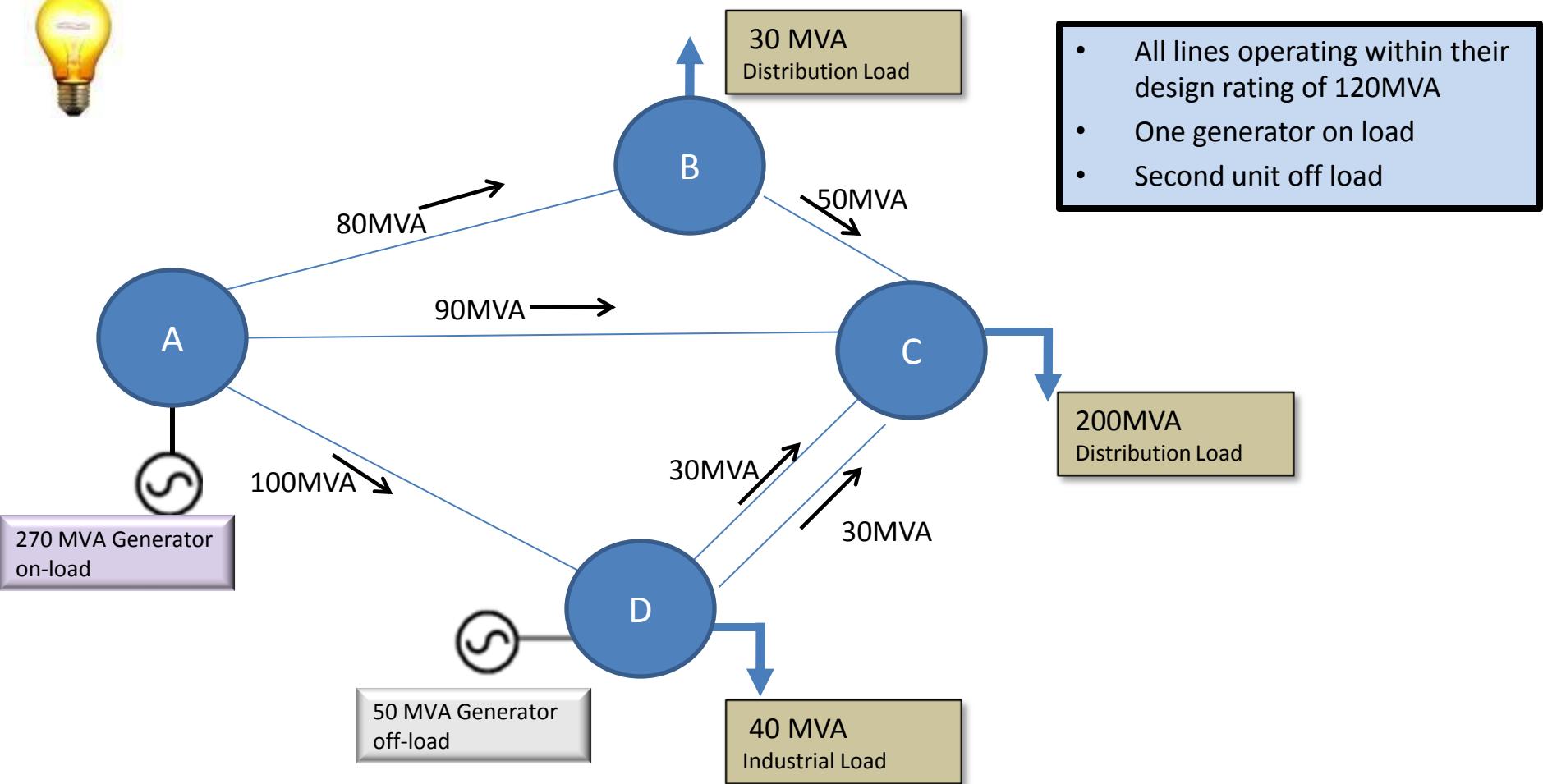


OPERATING A MESHEDE GRID: N-1 SECURITY

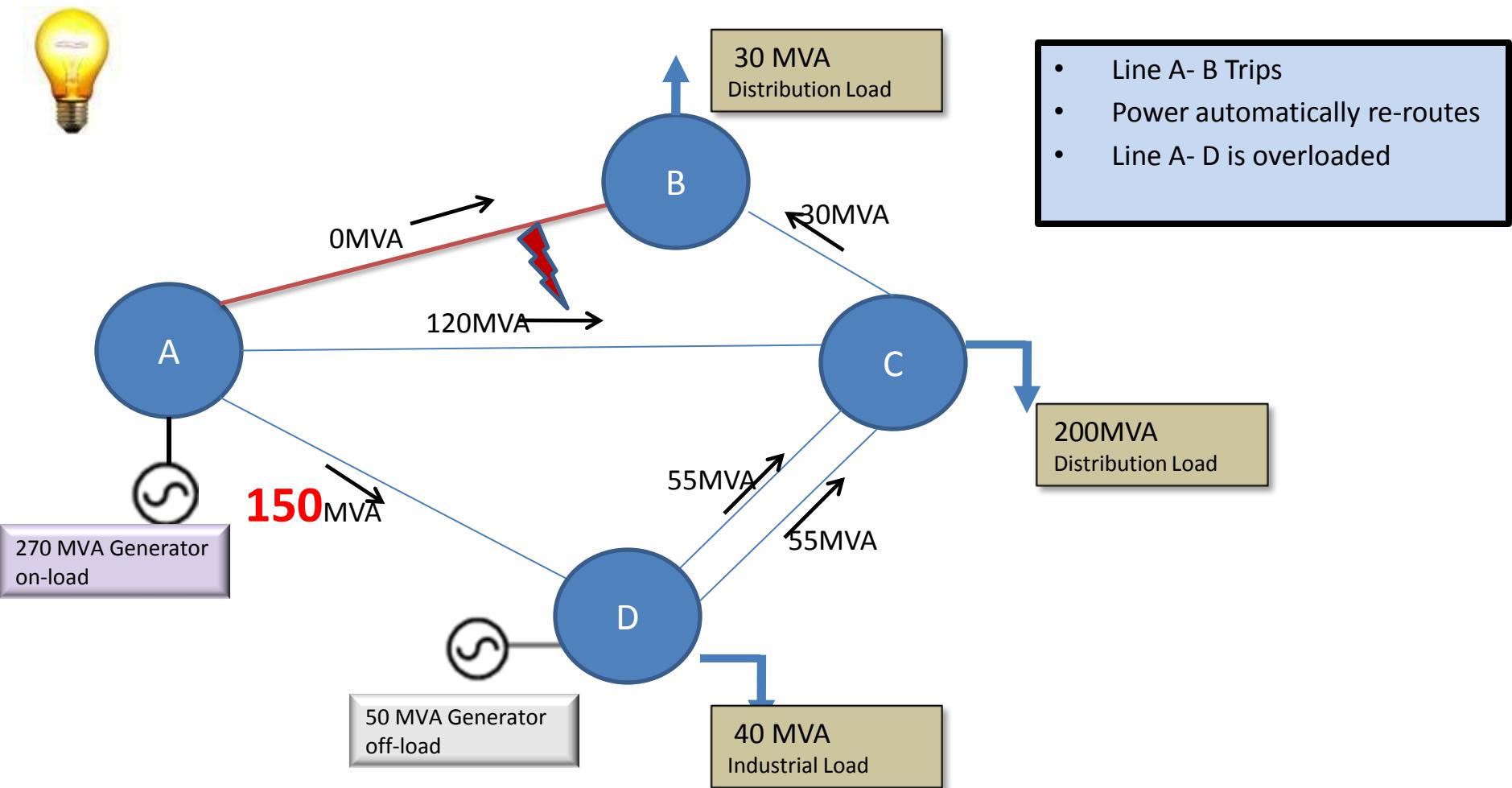
Meshed Grid Operation

- Power flows on lines varies in proportion to the impedance of the lines
- If a line is switched out power automatically re-routes down other in service lines
- This means there are no supply interruptions when a line is our for maintenance or trips....but
- NCC must ensure that *resulting* power flows are within acceptable limits

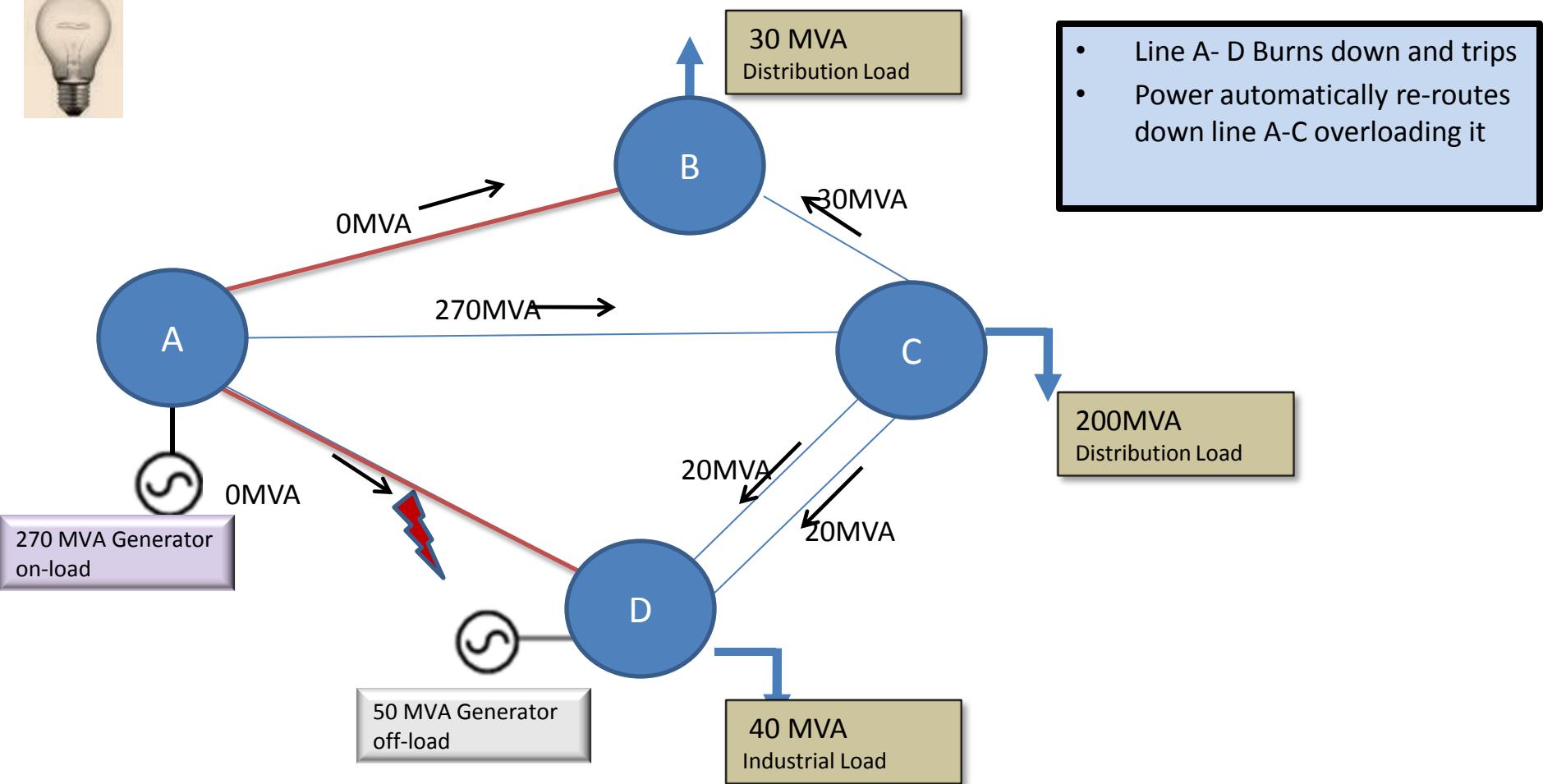
4 Bus System: Not N-1 Secure...Why?



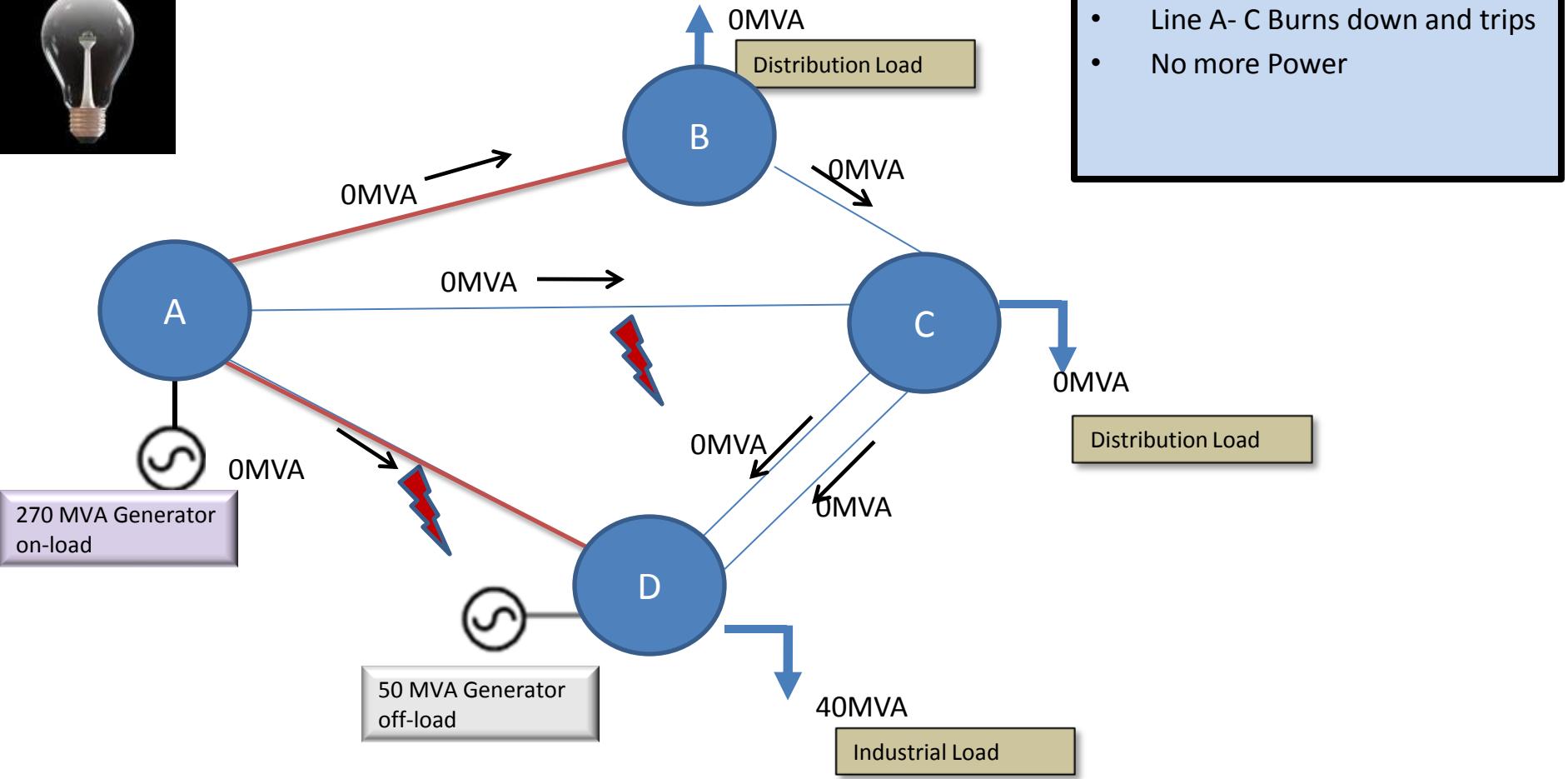
N-1 Event



Unsecure Network

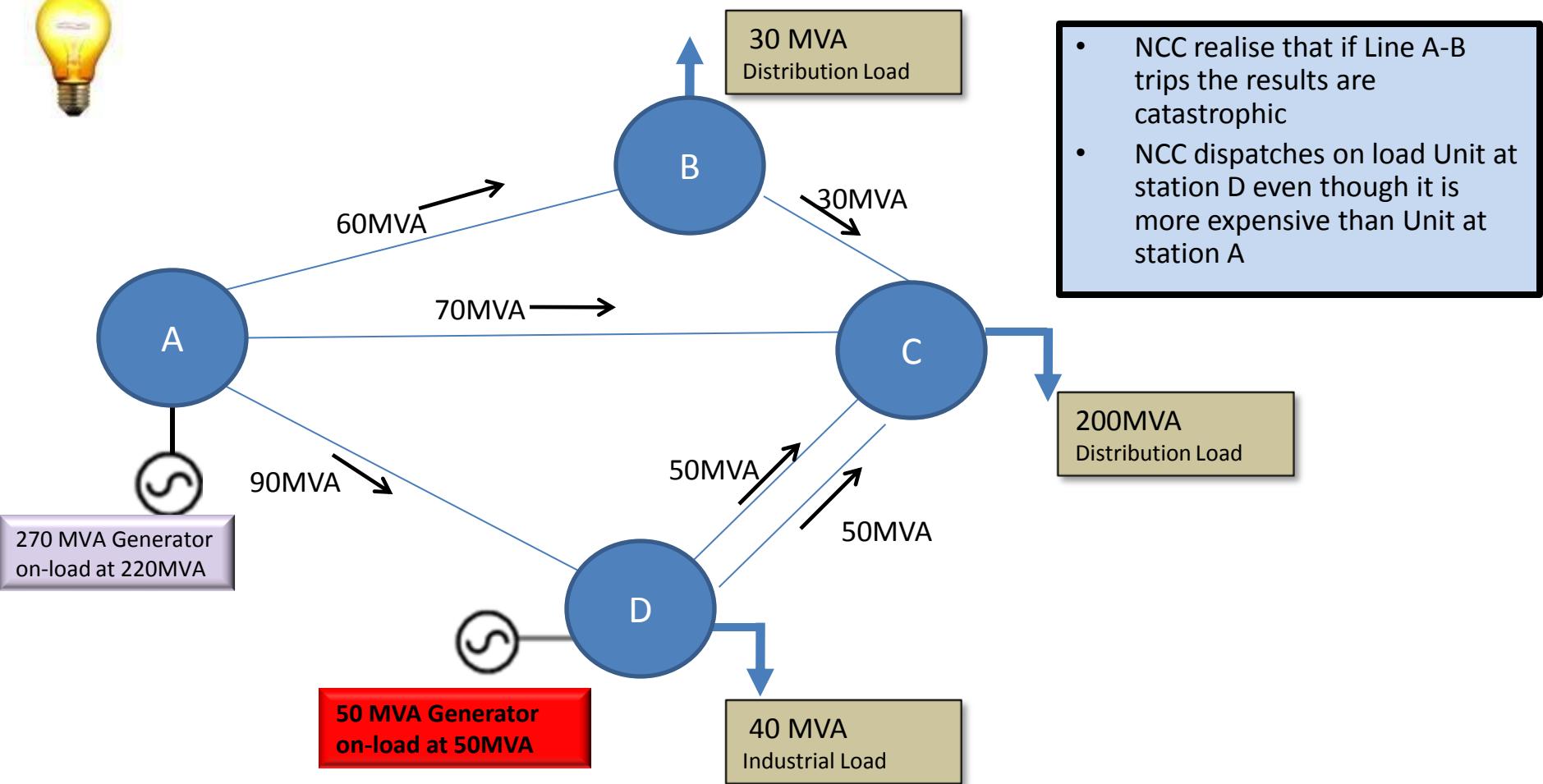


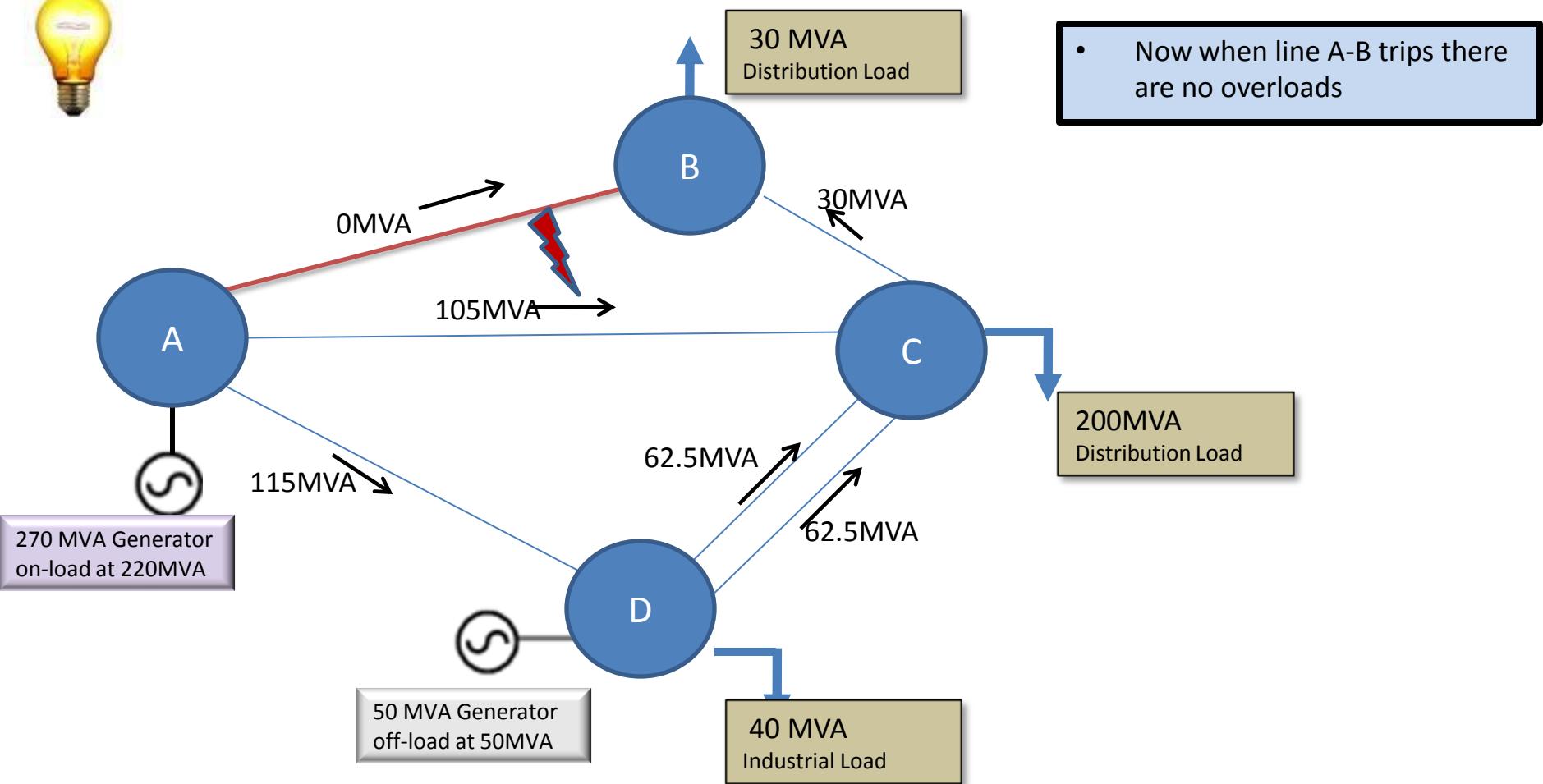
Blackout



What should have happened

N - 1 Secure





Enough Theory

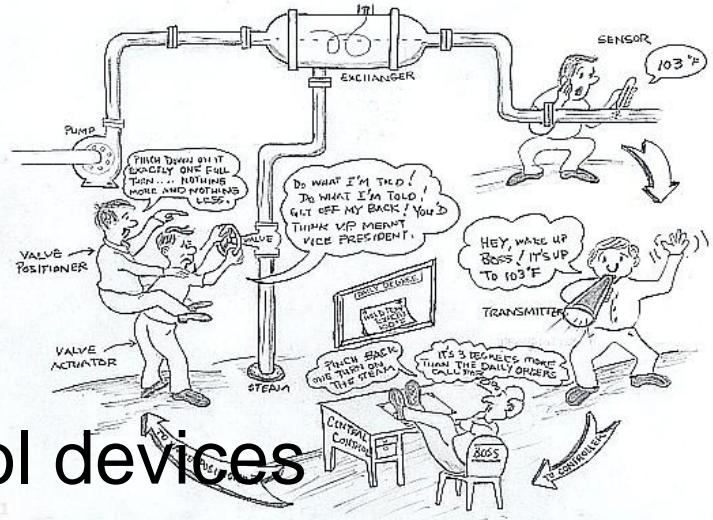
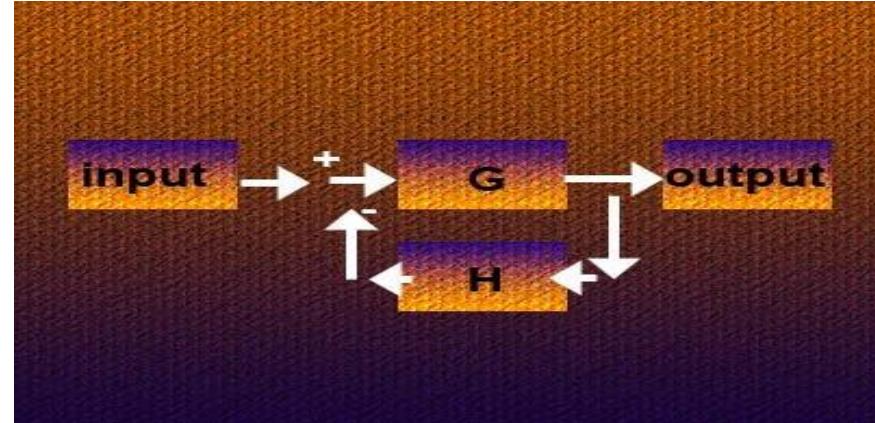
Transmission Engineer

- Monitors and controls voltage 
- Monitors and controls power flows 
- Responds to system alarms and events 
- Monitors the dynamic stability of the system
- Operational switching
 - Remote control
- Manages outages of transmission plant
- System restoration
- Manages connection of new or repaired equipment
 - Declarations of Fitness

VOLTAGE CONTROL

Voltage

- How is it monitored?
 - Set points, targets
 - Assessment tools
 - High visibility
- How is it implemented?
 - Range and scale of control devices
- Steady state v's transient control



Monitoring

- Voltage alarms
 - Trending
 - 4,900 measurement points
- On line voltage stability tool
 - Check voltage as load and topology changes
 - Are you over dependent on one generator?
- Contingency analysis
 - Check voltages as topology changes



Monitored

- Voltage monitored, alarmed and controlled within predefined ranges

Nominal Voltage	Base Case Limits	Post Contingency Limits
400 kV	370 to 410 kV	360 to 420 kV
220 kV	210 to 240 kV	200 to 245 kV
110 kV	105 to 120 kV	99 to 123 kV

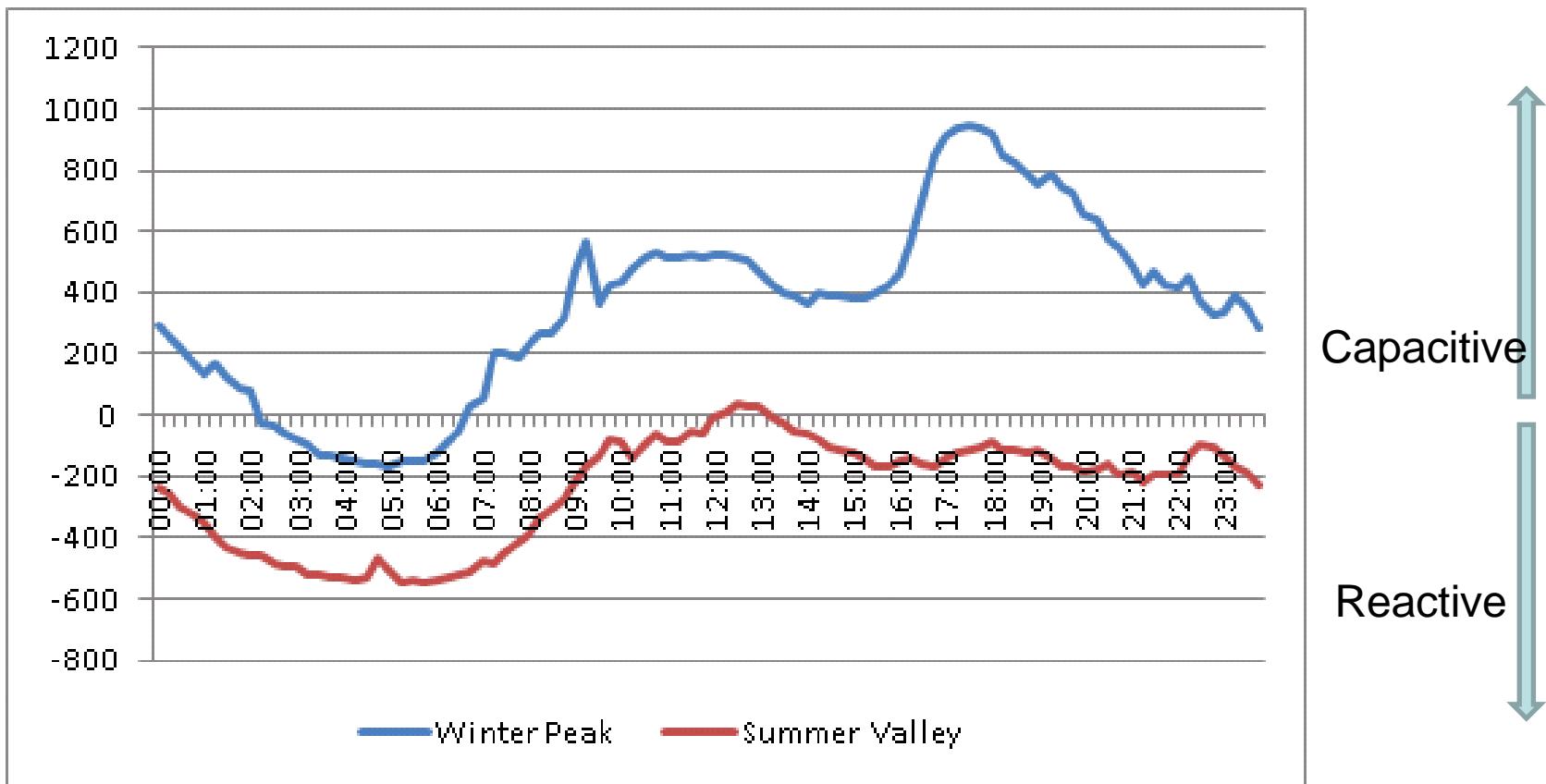
- <http://www.eirgrid.com/media/Operational%20Security%20Standards.pdf>

How is voltage controlled

- Generators
 - Dynamic source/sink
- Topology changes
 - Switching out cables
- Tap changing on transformers
 - Remote control
- Static reserve sources
 - Capacitors, Reactors



Reactive Power [MVar] Demand





Mon 07-Mar-2011 16:00:20 7.5 °C 50.00Hz

MVAR Overview

LLW

LAMP

ALERTS

SET	MVAR	VOLT	TAP	MAX LAG	MAX LEAD	SET	MVAR	VOLT	TAP	MAX LAG	MAX LEAD	SET	MVAR	VOLT	TAP	MAX LAG	MAX LEAD	
Aghada						Tur Hill						Sealrock						
AD1	0		15	153	-75	TH1	0	239		0	0	SK3	~	8	117	8	50	-32
AD2	-2		19	270	-150	TH2	0			0	0	SK4	~	8	117	8	50	-32
AT1	0			60	-37	TH3	0			0	0	G Island						
AT2	0	111		60	-37	TH4	0			0	0	GI1	—	0	117 ^R		42	0
AT4	0			60	-37							GI2	—	0		40	0	
DBP												GI3	—	0	235	82	-48	
DB1	~	19	238	4	295	-100												
HPL												Tarbert						
HNO	~	-3	111	7	107	-53						TB1	—	0	117		25	-10
HN1	~	4		181	-87							TB2	—	0		25	-7	
HN2	~	8	238	5	255	-170						TB3	—	0	236	18 ^R	110	-45
Marina												TB4	—	-1	19 ^R	110	-45	
MR1	—	0	117		0	0												
MRT	—	0			60	-32						Lanesboro						
M'Point												LR4	~	20	118	12	60	-20
MP1	~	20	408	4	176	-70						Shan'bridge						
MP2	~	11	400	4	176	-70						WO4	~	15	237	11	93	-60
MP3	~	20	406	4	176	-70						EPL						
			238									ED1	~	23	118	7 ^S	94	-50
Nth Wall												ED3	—	-1	118	40	0	0
NW4	—	0	239		0	0						ED5	—	0	118	1	38	0
NW5	—	0			65	-37												
Poolbeg												Rhode						
PB4	~	-2	239	14	80	-60						RP1	—	-1	116	7	32	-7
PB5	~	-6	238	16	80	-60						RP2	—	0	7	32	-7	
PB6	~	-4		14	130	-60												
Tynagh												Tawnaghmore						
TY1	~	-4	235	5	136	-87						TP1	—	-1	116		32	-7
TY2	~	10			102	-65						TP3	—	0	118		32	-7
Glanagow																		
WG1	~	20	238	7	282	-190												
Dublin & Cork MVAR Reserve																		
110																		
Lead Lag																		
Actual																		
Available																		
-3 103																		
-224 ^S 411 ^S																		
-832 ^S 1353 ^S																		
-210 528																		
-1266 ^S 2292 ^S																		
TOTAL																		
Lead Lag																		



Mon 07-Mar-2011 15:56:31

7.6 °C 50.03Hz

Transformer Tap & Cap. Overview

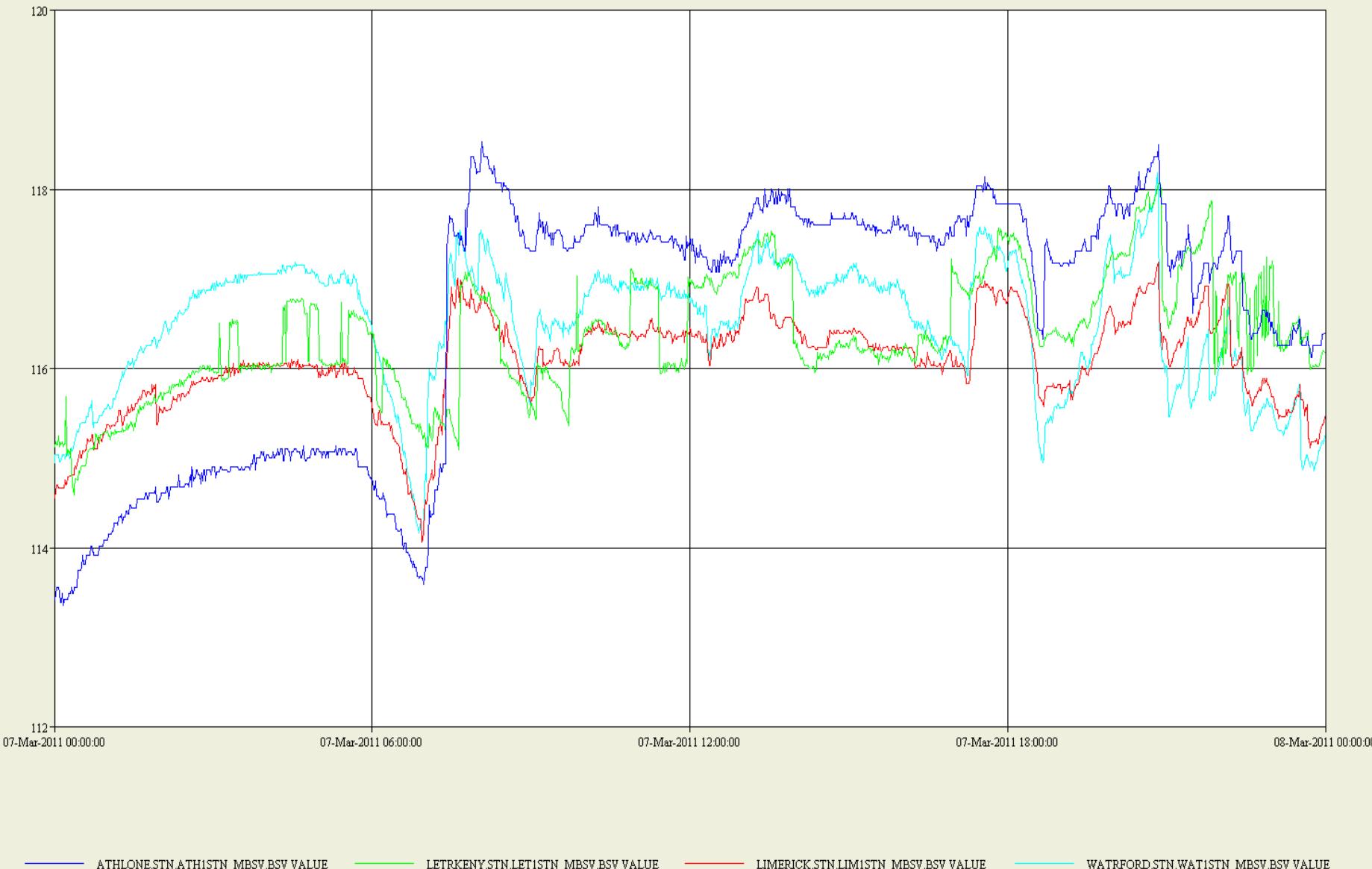
LLW LAMP

OCC_MASTER

Transformer	TAP	H/V	L/V	MW	MVAR	MVA	Transformer	TAP	H/V	L/V	MW	MVAR	MVA	CAPACITORS					
														STATUS	RATING	kV			
Dunstown							Kellis								Athlone Cap 1	—○—	30 MVar	118	
T4201	5	393	237	269	-7	269	T2101	5	237	116	37	3	37		Athlone Cap 3	◆—	30 MVar	118	
M'Point							T2102	5	238	115	37	3	38		Bandon Cap 1	◆—	15 MVar	119	
T4202	3	400	238	245	-41	249	Killonan	7	236	117	21	10	23		Cahir Cap 1	◆—	15 MVar	118	
Oldstreet							T2102	7	236	117	20	10	22		Cahir Cap 2	◆—	15 MVar	118	
T4202	9	405	236	17	-15	22	T2104	7	236	117	41	20	46		Cahir Cap 3	◆—	15 MVar	118	
Woodland							Knockraha								Cahir Cap 4	—○—	15 MVar	118	
T4201	5	398	238	197	4	197	T2101	6	236	117	95	13	96		Cashla Cap 1	◆—	40 MVar	117	
T4202	5	0	0	0	0	0	T2102	6	237	117	95	13	96		Cashla Cap 2	—○—	40 MVar	117	
Aghada							Louth								Castlebar Cap 2	—○—	30 MVar	117	
T2102	5	241	118	27	-3	27	AT1	9R	283	237	-18	-1	-18		Cath Fall Cap 2	◆—	15 MVar	117	
Arklow							AT2	9	281	237	-36	4	-36		Dalton Cap 1	◆—	15 MVar	117R	
T2101	5	234	118	25	3	25	AT3	9	283	237	-18	0	-18		Doon Cap 1	◆—	15 MVar	117	
T2102	6	234	118	38	2	38	T2101	6	238	117	33	3	33		Drumline Cap 2	◆—	15 MVar	116	
Ck'mines							T2102	6	238	117	32	6	33		Dunmanway Cap 2	◆—	15 MVar	118	
T2101	6	237	117	103	23	105	T2103	6	237	117	32	4	32		Gortawee Cap 1	◆—	15 MVar	117	
T2102	6	239	117	102	22	105	T2104	6	237	117	67	19	70		Kilkenny Cap 2	◆—	30 MVar	116R	
Cashla							Maynooth								Kilteel Cap 1	—○—	30 MVar	117	
T2101	5	237	118	101	-18	102	T2101	6	240	118	24	7	25		Letterkenny Cap 2	◆—	15 MVar	116R	
T2102	5	238	117	103	-21	105	T2102	6	239	118R	50	18	53		Louth Cap 1	—○—	30 MVar	118	
T2104	5	236	117	48	-8	49	T2103	6	240	118	18	6	19		Moy Cap 1	—○—	15 MVar	115	
Clashavoon							T2104	6	238	118	39	14	41		Moy Cap 2	◆—	15 MVar	115	
T2101	5	238	117	58	-7	59	Poolbeg								Navan Cap 1	◆—	30 MVar	116	
Corduff							TF3	5	240	116	118	15	119		Raffeen Cap 2	◆—	60 MVar	118	
T2101	6	238	118	109	9	110	TF4	5	240	116	111	11	112		Shankill Cap 2	◆—	30 MVar	116	
T2102	6	238	118	112	14	113	Raffeen								Sligo Cap 1	◆—	15 MVar	116	
Cullenagh							T2101	5	240	118	70	-4	70		Thurles Cap 1	◆—	15 MVar	118	
T2101	5	237	117	81	-5	81	T2102	5	240	119	85	-31	91		Tralee Cap 2	◆—	30 MVar	117	
Finglas							Shan'bridge								Trien Cap 1	—○—	30 MVar	117	
T2101	6	240	119	92	-1	92	T2101	5	238	116	10	-4	11		Wexford Cap 2	◆—	15 MVar	116	
T2102	6	240	120	92	0	92	T2102	5	238	116	10	-5	11		Wexford Cap 4	—○—	15 MVar	116	
T2103	6	239	119	74	23	78	Tarbert												
T2104	6	238	118R	75	18	77	T2101	5	237	117	50	-16	52						
T2106	6	240	119	0	0	0	T2102	5	237	117	51	-16	53						
Flagford																			
T2101	5	238	117	56	-7	57													
T2102	5	238	119	60	-6	61													
Gorman																			
T2101	6	237	117	63	-9	64													
G Island																			
T2101	6R	237	117	46	8	47													

TRANSFORMER
BARGRAPH VIEW

110kV profiles - Start: 07-Mar-2011 00:00:00



ATHLONE.STN.ATH1STN_MBSV.BSV VALUE

LETRKENY.STN.LET1STN_MBSV.BSV VALUE

LIMERICK.STN.LIM1STN_MBSV.BSV VALUE

WATRFORD.STN.WAT1STN_MBSV.BSV VALUE

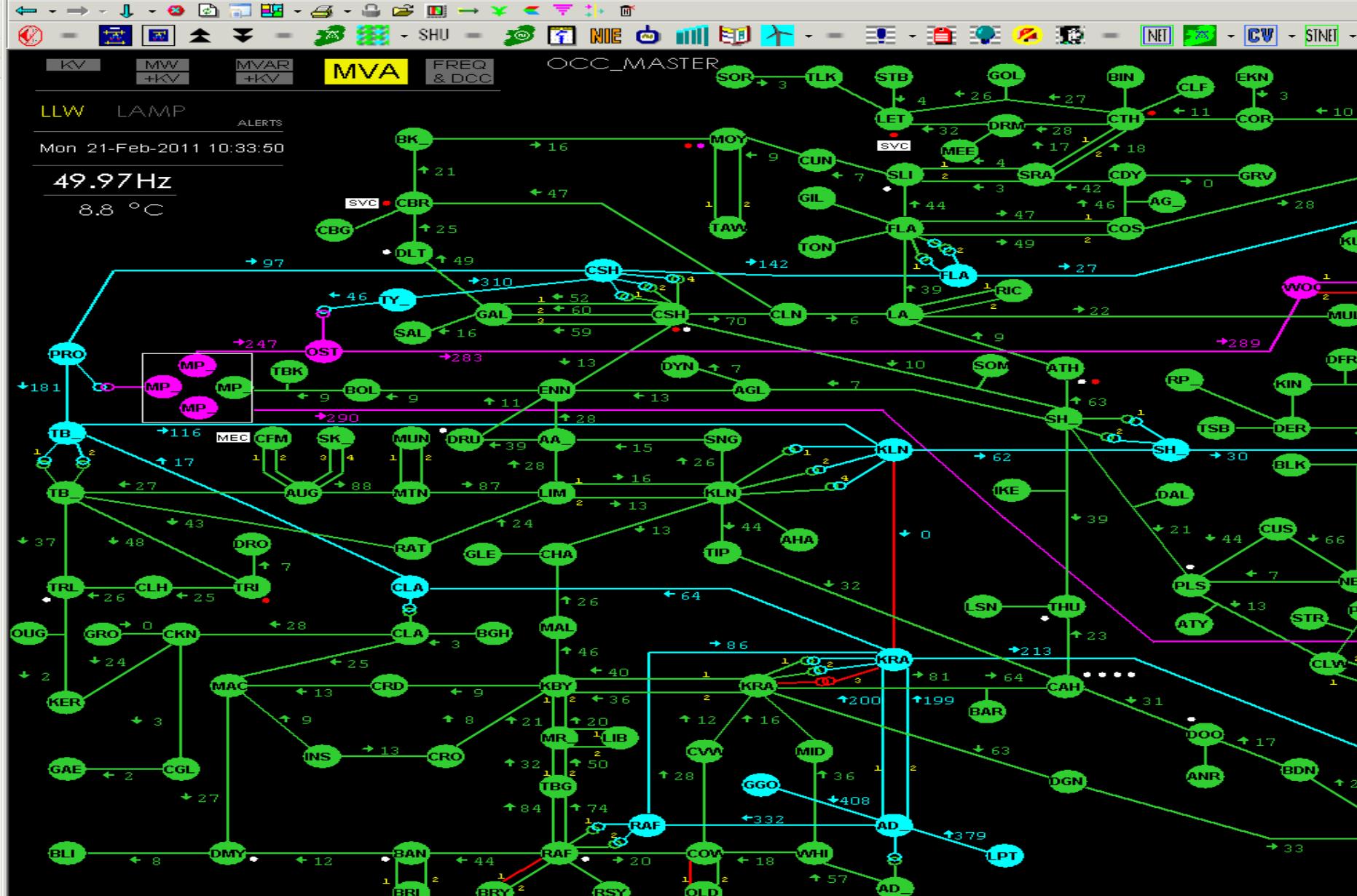
A SINGLE CABLE FAULT EFFECTS THE ENTIRE SYSTEM

Inchicore – Irishtown 220kV cable fault at 09:28 on 27 January 2007



- Transient voltage response
- Protection operated to clear the fault in 0.05 of a second
- Fault isolated and system integrity preserved
- Over 350 alarms triggered on the EMS System in 10 seconds
- Required on-going operational measures in Dublin (sectionalising and generation re-dispatch)

POWER FLOW



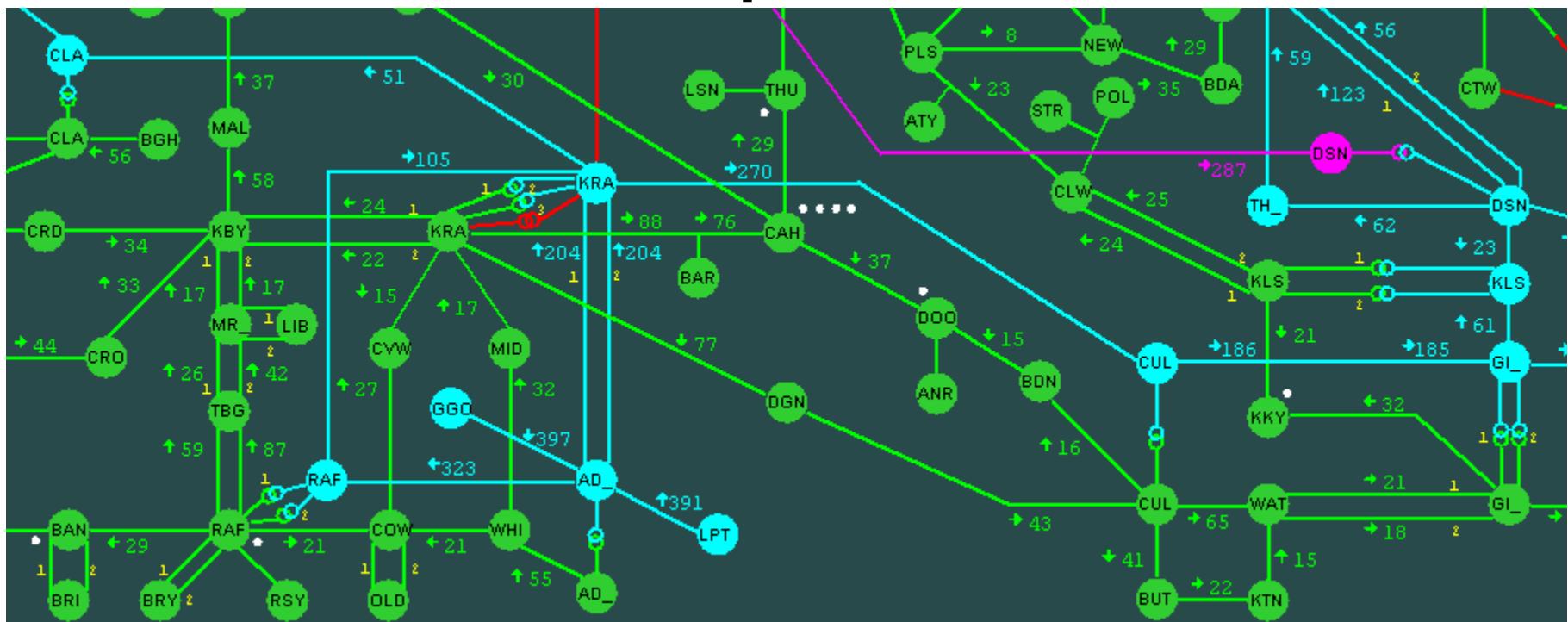
Monitoring Power Flows

- Line flows alarmed
 - Endangered and Disturbed levels
- Contingency Analysis
 - N-1 analysis
- Study environment
 - Can be used to examine future events

Controlling Power Flow

- Generation commitment and dispatch
 - Out of merit generation required
- Change topology
 - Sectionalise the network
 - Trade off with security
 - Phase shifting transformers
- Load transfer
- Load shedding

Example Case



Load 3560 MW (3pm on an average Monday in March)

Medium wind – 251 MW

Cork Generation – 800 MW

Cullenagh – Waterford 110 kV line (rated 116 MVA)

Contingency Violation

Contingency Violations		Contingency Violations:		Summary	Branch	Voltage	Angle	Interface	
				Summary	Branch	Voltage	Angle	Interface	
				Study	Run	STNET	STUDY	COMPLETE	
Values Bar									UNSOVED CTG: 1
Alarm New Warn				Type	Volt Class	Pre CTG Value	Postctg Value	Rating	
%						LN: XF: ZBR:	MVA MVA MVA	AMP AMP AMP	MVA MVA MVA
100	110	120	130	140	150				
CTG: MP_40ST1 MONEYPPNT - OLDESTRET 400KV LINE █ █ █ VIOL: DUNSTOWN TRANSF DSN4T421NTTX BR 380 277.7 455.7 674									
CTG: INC2T211 INCHICOR T2101 220/110KV TRAFO █ █ █ VIOL: INCHICOR TRANSF INC2T212NTTX BR 220 115.4 236.1 577									
CTG: INC2T212 INCHICOR T2102 220/110KV TRAFO █ █ █ VIOL: INCHICOR TRANSF INC2T211NTTX BR 220 115.4 236.1 577									
CTG: PB_2TF_3 POOLBEG TF3 220/110KV TRAFO █ █ █ VIOL: POOLBEG TRANSF PB_2T214NTTX BR 220 113.1 228.5 557									
CTG: PB_2TF_4 POOLBEG TF4 220/110KV TRAFO █ █ █ VIOL: POOLBEG TRANSF PB_2T213NTTX BR 220 113.1 228.5 557									
CTG: CUL2GI_1 CULLNAGH - GTISLAND 220KV LINE █ █ █ VIOL: CUL1WAT1NFDR @CULLNAGH BR 110 66.4 141.5 710 116									
CTG: CUL2KRA1 CULLNAGH - KNOCKRAHA 220KV LINE █ █ █ VIOL: BCK1KRA1NFDR @KNOCKRAHA BR 110 88.0 140.3 697									

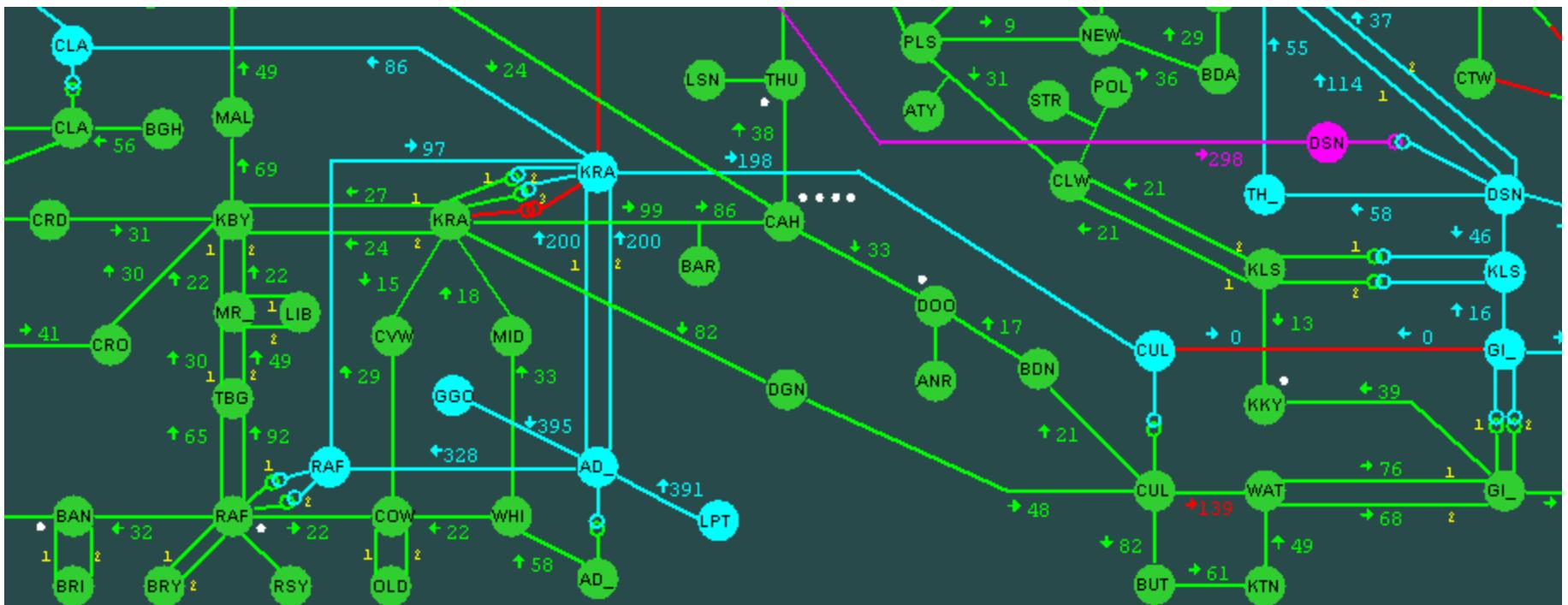
Contingency Analysis Warning

Loss of Cullenagh – Great Island 220 kV line

>121 % overload on Cullenagh – Waterford 110 kV line (rated 116 MVA)

60 MW reduction of Cork generation required to comply with operating standards

East - West Contingency



Tripping of Cullenagh – Great Island 220 kV line

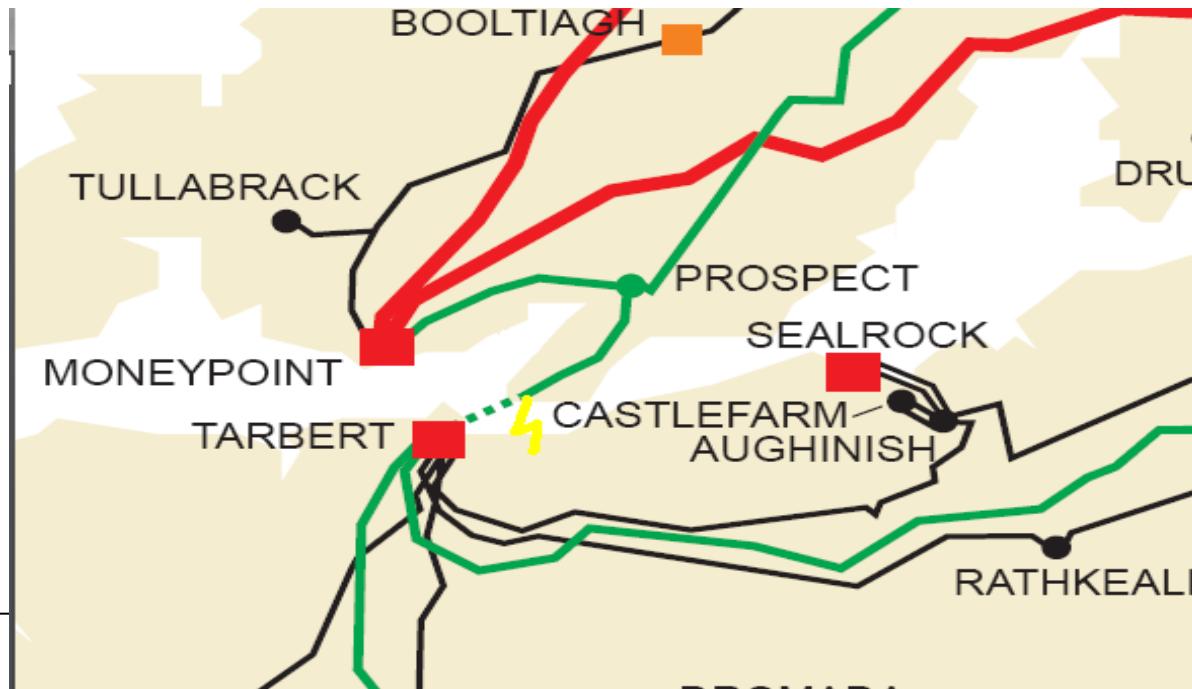
-> 121 % overload on Cullenagh – Waterford 110 kV line

139 MVA flowing on a 116 MVA rated line

REAL LIFE FAULTS

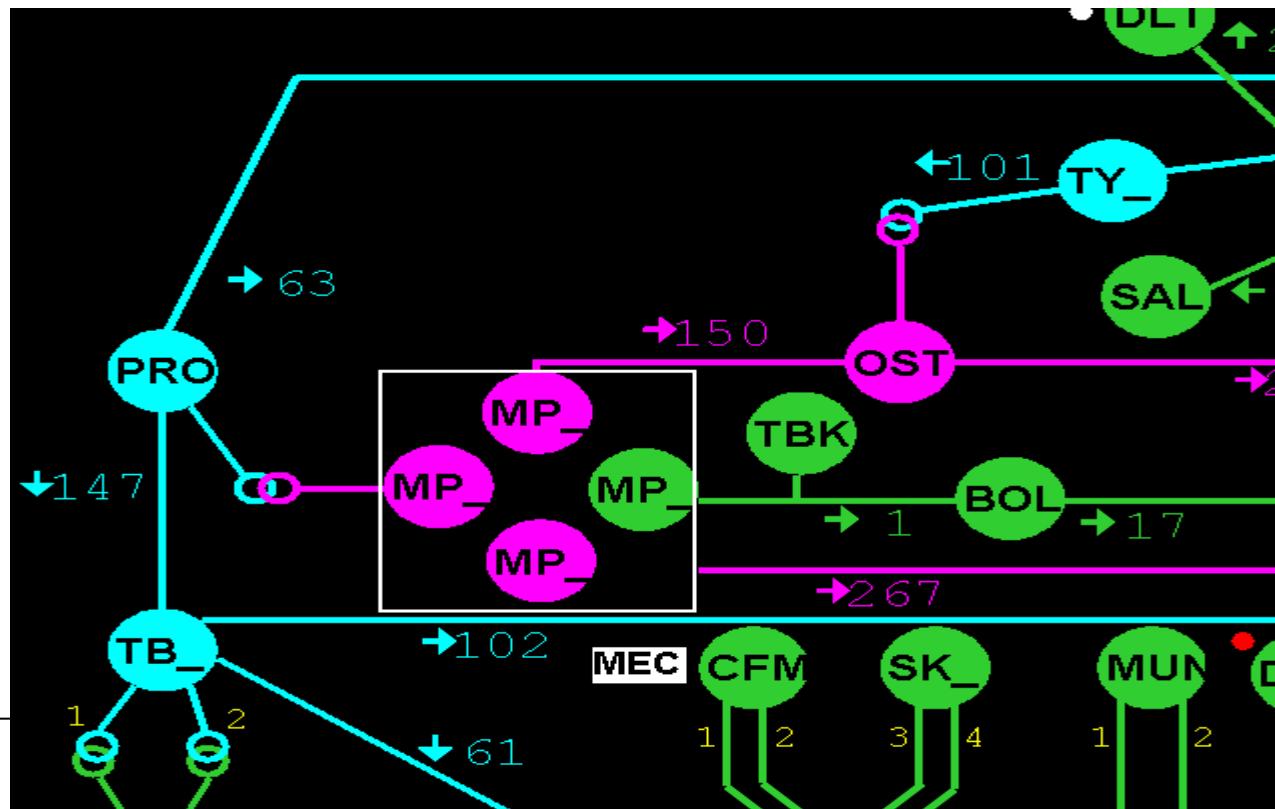
Transmission Fault

- Prospect Tarbert 220 kV line made up of 7.65 km of 220 kV OHL from Prospect and 2 km UGC under the Shannon to Tarbert
- At 16:00:49 on 4th Feb 2011 - a fault occurred on T phase of the feeder



Pre-fault Operational Info

- 147 MW flowing from Prospect to Tarbert
- 240 kV at Prospect busbar 238 kV at Tarbert busbar



Alarms

04-feb-2011 16:00:50 s TRIEN 110KV CLAHANE 1 REL521 DCEF REV PU ON
 04-feb-2011 16:00:50 s TRIEN 110KV DROMADA 1 7SA612 NEUTRAL PU ON
 04-feb-2011 16:00:50 s TRIEN 110KV DROMADA 1 7SA612 DCEF REV PU ON
 04-feb-2011 16:00:51 s AUGHINIS 110KV TARBERT 1 REL DCEF TX ON
 04-feb-2011 16:00:51 s DROMADA 110KV TRIEN 1 7SA6 NEUTRAL PU ON
 04-feb-2011 16:00:51 s DROMADA 110KV TRIEN 1 7SA6 DCEF TX ON
 04-feb-2011 16:00:51 s AUGHINIS 110KV TARBERT 1 REL DCEF TX OFF
 04-feb-2011 16:00:51 s KILLONAN 220KV TARBERT 1 E/F PU LEVEL ON
 04-feb-2011 16:00:51 s TRALEE 110KV TARBERT 1 7SN20 EF PU LVL ON
 04-feb-2011 16:00:51 s CLSHVOON 220KV KRAHA 1 7SA513 DCEF TRIP ON
 04-feb-2011 16:00:51 s TYNAGH 220KV GENERAL STATION ALARM ON
 04-feb-2011 16:00:51 s SINGLAND 110KV ARDNA 1 REL DCEF REVPU ON
 04-feb-2011 16:00:51 s DROMADA 110KV TRIEN 1 7SA6 NEUTRAL PU OFF
 04-feb-2011 16:00:51 s DROMADA 110KV TRIEN 1 7SA6 DCEF TX OFF
 04-feb-2011 16:00:52 s TRIEN 110KV DROMADA 1 7SA612 DCEF RX ON
 04-feb-2011 16:00:52 s TRIEN 110KV CLAHANE 1 REL521 DCEF REV PU OFF
 04-feb-2011 16:00:52 s TRIEN 110KV DROMADA 1 7SA612 NEUTRAL PU OFF
 04-feb-2011 16:00:52 s TRIEN 110KV DROMADA 1 7SA612 DCEF RX OFF
 04-feb-2011 16:00:52 s TRIEN 110KV DROMADA 1 7SA612 DCEF REV PU OFF
 04-feb-2011 16:00:52 s MUJNGAMMINANE CB 20KV T421 CCT BRK STTS OPEN
 04-feb-2011 16:00:53 s TRALEE 110KV TARBERT 1 7SA511 T PH PU ON
 04-feb-2011 16:00:53 s TRALEE 110KV TARBERT 1 7SA511 ETH PU ON
 04-feb-2011 16:00:53 s TRALEE 110KV TARBERT 1 7SN20 EF PT TX ON
 04-feb-2011 16:00:53 s KILLONAN 220KV TARBERT 1 E/F TRIP LEVEL ON
 04-feb-2011 16:00:53 s TRALEE 110KV TARBERT 1 7SA511 T PH PU OFF
 04-feb-2011 16:00:53 s TRALEE 110KV TARBERT 1 7SA511 ETH PU OFF
 04-feb-2011 16:00:53 s TRALEE 110KV TARBERT 1 7SN20 EF PT TX OFF
 04-feb-2011 16:00:53 s TRALEE 110KV TARBERT 1 7SN20 EF PU LVL OFF
 04-feb-2011 16:00:53 s CUNGHILL CB 20KV CAP STEP 1 CCT BRK STTS CLOSED
 04-feb-2011 16:00:53 s CLSHVOON 220KV TARBT 1 7SA513 T PH PU ON
 04-feb-2011 16:00:53 s KNOCKAWARRIGA CB 20KV T421 CCT BRK STTS OPEN
 04-feb-2011 16:00:53 s SINGLAND 110KV GENERAL STATION ALARM ON
 04-feb-2011 16:00:53 s SINGLAND 110KV ARDNA 1 REL DCEF REVPU OFF
 04-feb-2011 16:00:53 s CASHLA 220KV PROSPECT 1 7SA T PHASE PU ON
 04-feb-2011 16:00:53 s CASHLA 220KV TYNAGH 1 DCEF PU LEVEL ON
 04-feb-2011 16:00:53 s CASHLA 220KV TYNAGH 1 DCEF TRIP LEVEL ON
 04-feb-2011 16:00:53 s BALNCOGL NETWORKS 7SA J1 FAULT ON
 04-feb-2011 16:00:53 s CASHLA 220KV PROSPECT 1 7SA T PHASE PU OFF
 04-feb-2011 16:00:53 s CASHLA 220KV TYNAGH 1 DCEF PU LEVEL OFF
 04-feb-2011 16:00:53 s CASHLA 220KV GENERAL STATION ALARM ON
 04-feb-2011 16:00:53 s TARBERT 110KV AUGHINIS 1 REL DCEF REV PU ON
 04-feb-2011 16:00:53 s TARBERT 220KV TRIEN 1 REL521 DCEF REV PU ON
 04-feb-2011 16:00:53 s TARBERT 220KV PROSPECT 1 EARTH PICKUP ON
 04-feb-2011 16:00:53 s TARBERT 220KV CLSHVOON 1 T PHASE PICKUP ON
 04-feb-2011 16:00:53 s TARBERT 220KV CLSHVOON 1 T PHASE PICKUP ON
 04-feb-2011 16:00:53 s TARBERT 220KV T2101 7SA612 NEUTRAL PU ON
 04-feb-2011 16:00:53 s TARBERT 220KV T2101 7SA612 NEUTRAL PU ON
 04-feb-2011 16:00:53 s BALNCOGL NETWORKS 7SA J1 FAULT OFF
 04-feb-2011 16:00:53 s KILLONAN 220KV TARBERT 1 T PHASE PICKUP ON
 04-feb-2011 16:00:53 s KILLONAN 220KV TARBERT 1 E/F PER TRP TX ON
 04-feb-2011 16:00:53 s KILLONAN 110KV SINGLAND 1 REL REV E/F PU ON
 04-feb-2011 16:00:53 s CLSHVOON 220KV KRAHA 1 7SA513 EARTH PU ON
 04-feb-2011 16:00:53 s CLSHVOON 220KV TARBT 1 7SA513 DCEF TRIP ON
 04-feb-2011 16:00:53 s CLSHVOON 220KV TARBT 1 7SA513 EARTH PU ON
 04-feb-2011 16:00:53 s CLSHVOON 220KV TARBT 1 7SA513 DCEF TRIP ON
 04-feb-2011 16:00:53 s KILLONAN 220KV TARBERT 1 E/F PU LEVEL OFF
 04-feb-2011 16:00:53 s KILLONAN 220KV TARBERT 1 E/F TRIP LEVEL OFF
 04-feb-2011 16:00:53 s KILLONAN 220KV TARBERT 1 T PHASE PICKUP OFF
 04-feb-2011 16:00:53 s KILLONAN 220KV TARBERT 1 E/F PER TRP TX OFF
 04-feb-2011 16:00:55 s PROSPECT 220KV TARBERT 1 7SA POTT RX OFF
 04-feb-2011 16:00:55 s PROSPECT 220KV TARBERT 1 7SA POTT TX OFF
 04-feb-2011 16:00:55 s PROSPECT 220KV TARBERT 1 7SA DCEF RX OFF
 04-feb-2011 16:00:55 s PROSPECT 220KV TARBERT 1 7SA DIST TRIP OFF
 04-feb-2011 16:00:55 s PROSPECT 220KV TARBERT 1 7SA DCEF TRIP OFF
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA NEUTRAL PU OFF
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA 1P TRIP ON
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA DCEF TRIP ON
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA POTT RX ON
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA DIST TRIP ON
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA T PHASE PU OFF
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA NEUTRAL PU OFF
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA POTT TX OFF
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA DCEF RX OFF
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA DIST TRIP OFF
 04-feb-2011 16:01:02 s PROSPECT 220KV TARBERT 1 7SA DCEF TRIP OFF
 04-feb-2011 16:01:07 s KNOCRHA 220KV CLSHVOON 1 7SA DCEF PU LV OFF



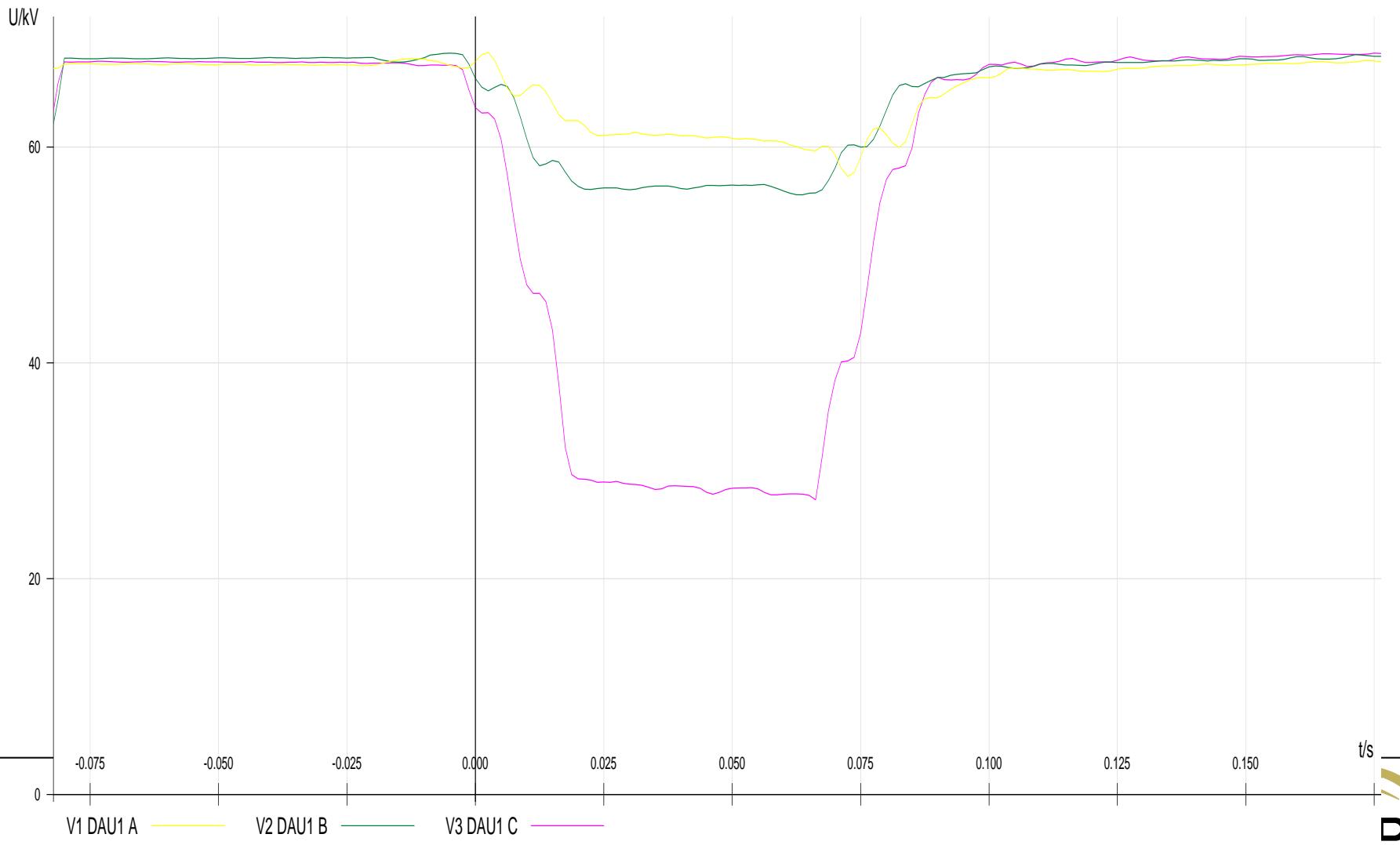
Protection Operations - Prospect

- Total fault clearance time: 80 milliseconds
- The relay in Prospect indicated that the fault was close to or on the cable section of the feeder.
 - Auto restoration is blocked for such faults.
- Follow up inspections indicated
 - No issue with the cable section.
 - A failed surge arrestor at the line/cable interface



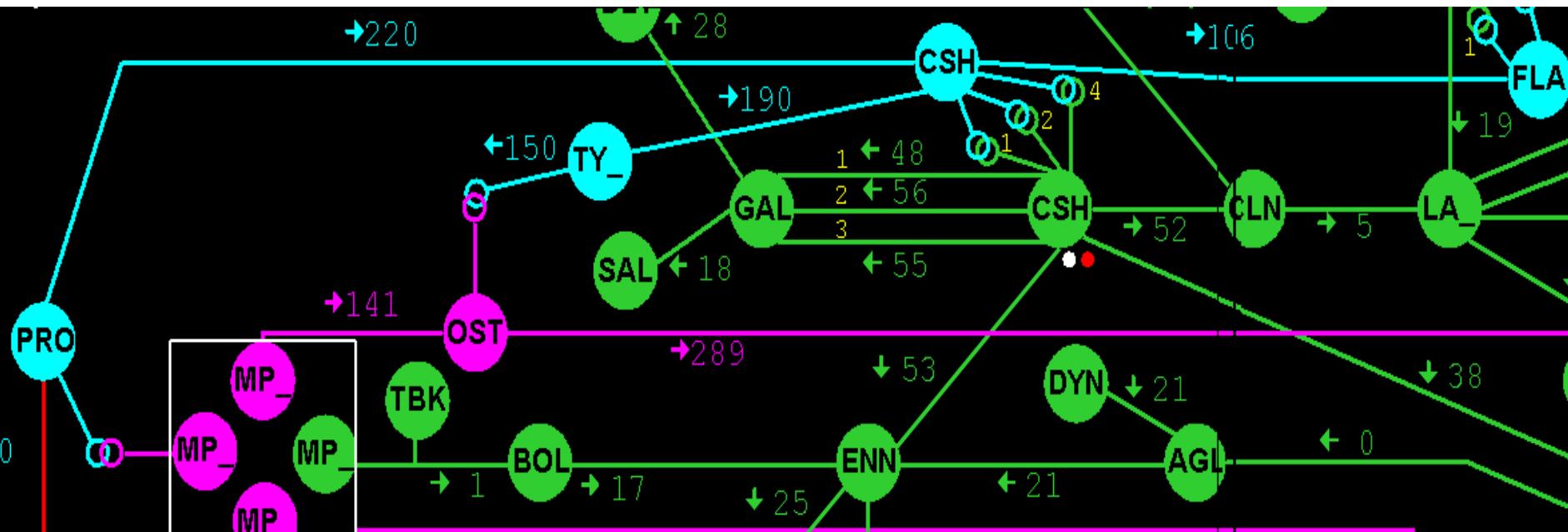
Voltage Dip in Dromada 110kV - Kerry

RMS R, S, T Voltages during the fault taken from T121 in Dromada



Post-fault Operational

- 147 MW power flow from Moneypoint to Prospect gets redirected to Cashla after the Tarbert line trips
- This was fed back to the south network via the 110 kV lines in Cashla and Flagford
- There was no line overloads as a result of the line tripping



Post Fault Actions

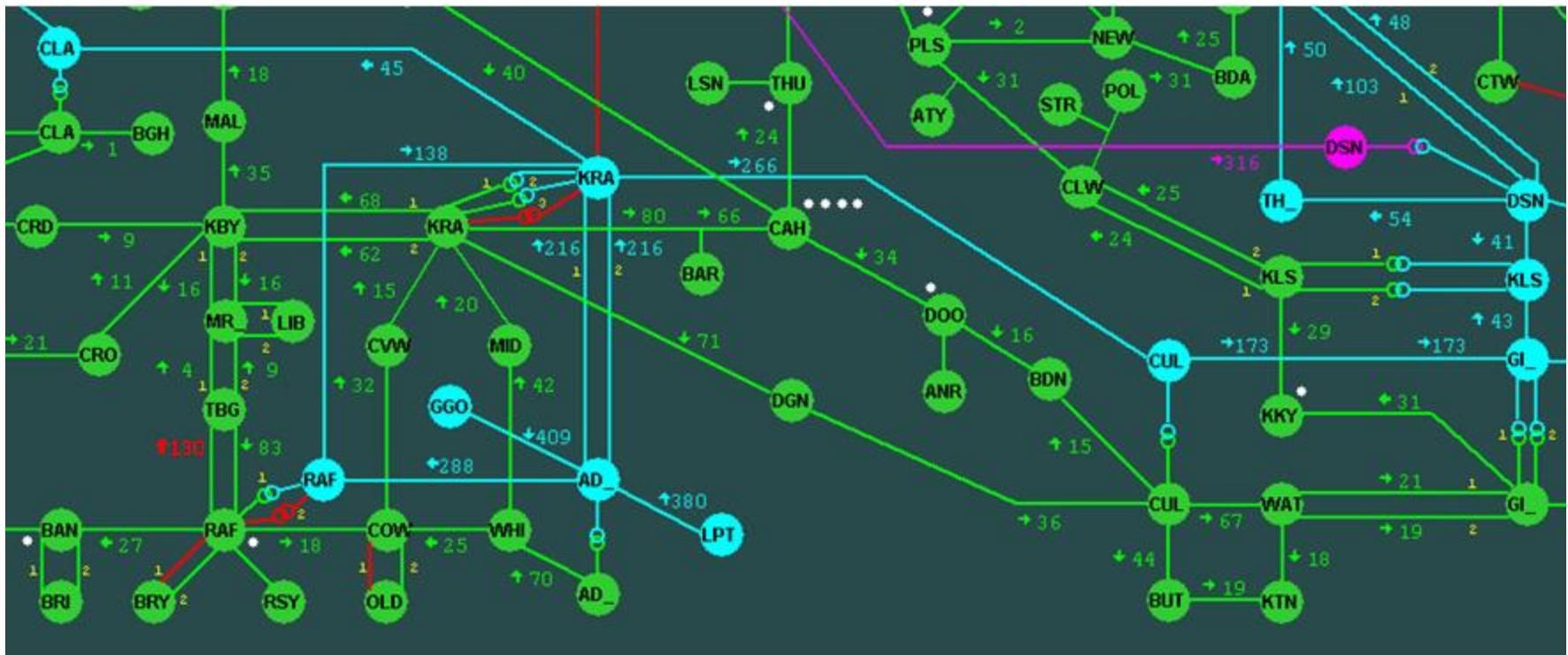
- New surge arresters installed and tested at the line cable interface on 6th of February.
- Feeder was returned to service at 18:53 hours on the 6th of February

High Impact Low Probability Event

Shannonbridge
27th Feb 2011

End

Cork 110 kV Contingency



Loss of Raffeen T2102 220/110 kV transformer

-> overload on Raffeen – Trabeg 1 (one) 110 kV line

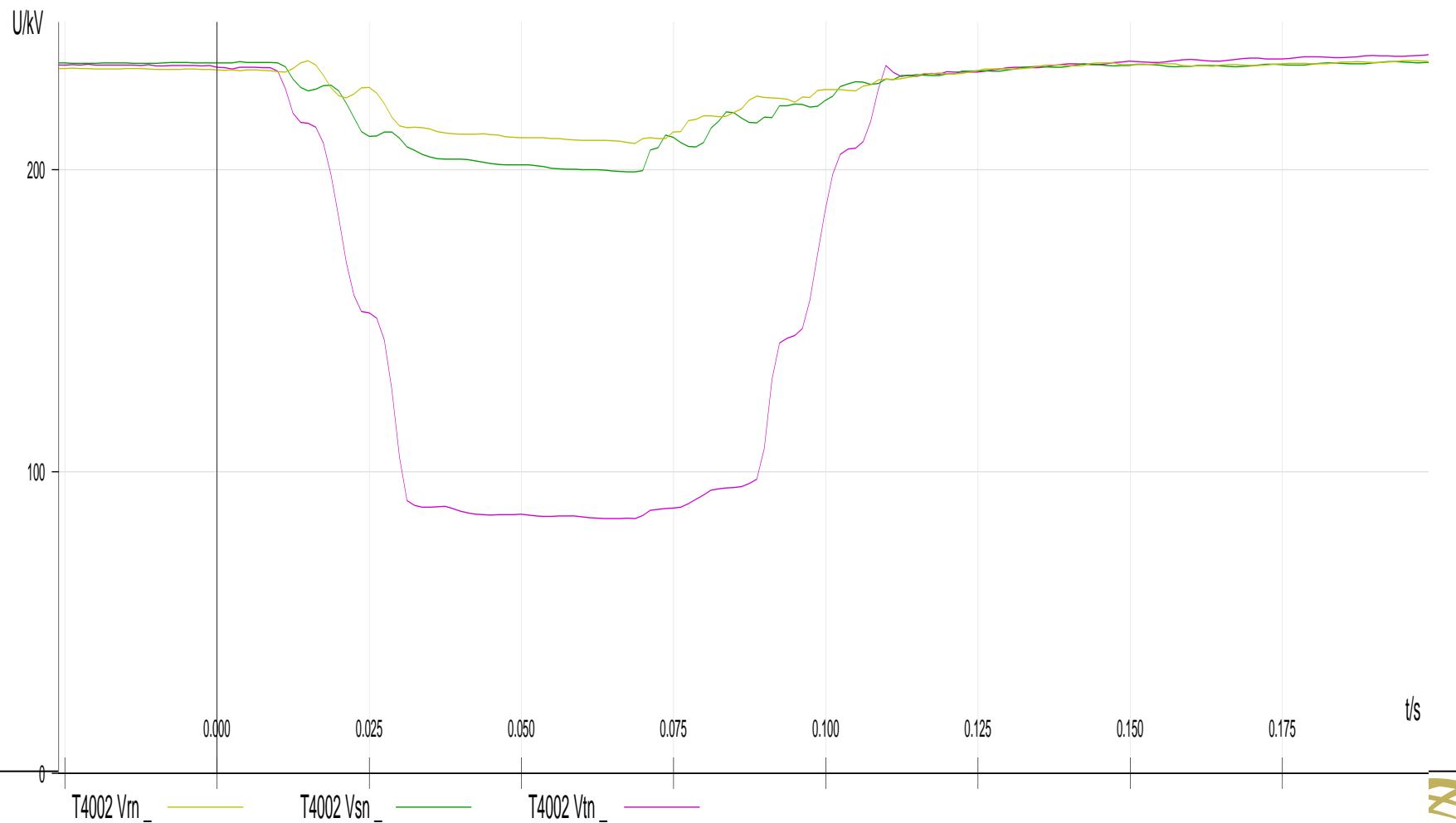
113 % overload on 116 MVA rated line

Voltage dips during the fault

- At the Prospect Side
 - In Moneypoint the 400 kV T phase voltage dipped from 235kV -> 84 kV (35.7 % retained)
 - In Cashla the 220 kV T phase voltage dipped from 138 kV -> 115.7 kV (83.8 % retained)
- At the Tarbert Side
 - In Dromada the 110 kV T phase voltage dipped from 67.9 kV -> 27.4 kV (40.4 % retained)
 - In Clashavoon the 220 kV T phase voltage dipped from 138.9 kV -> 79.2 kV (57 % retained)
 - In Longpoint the 220 kV T phase voltage dipped from 140 kV -> 106 kV (76 % retained)

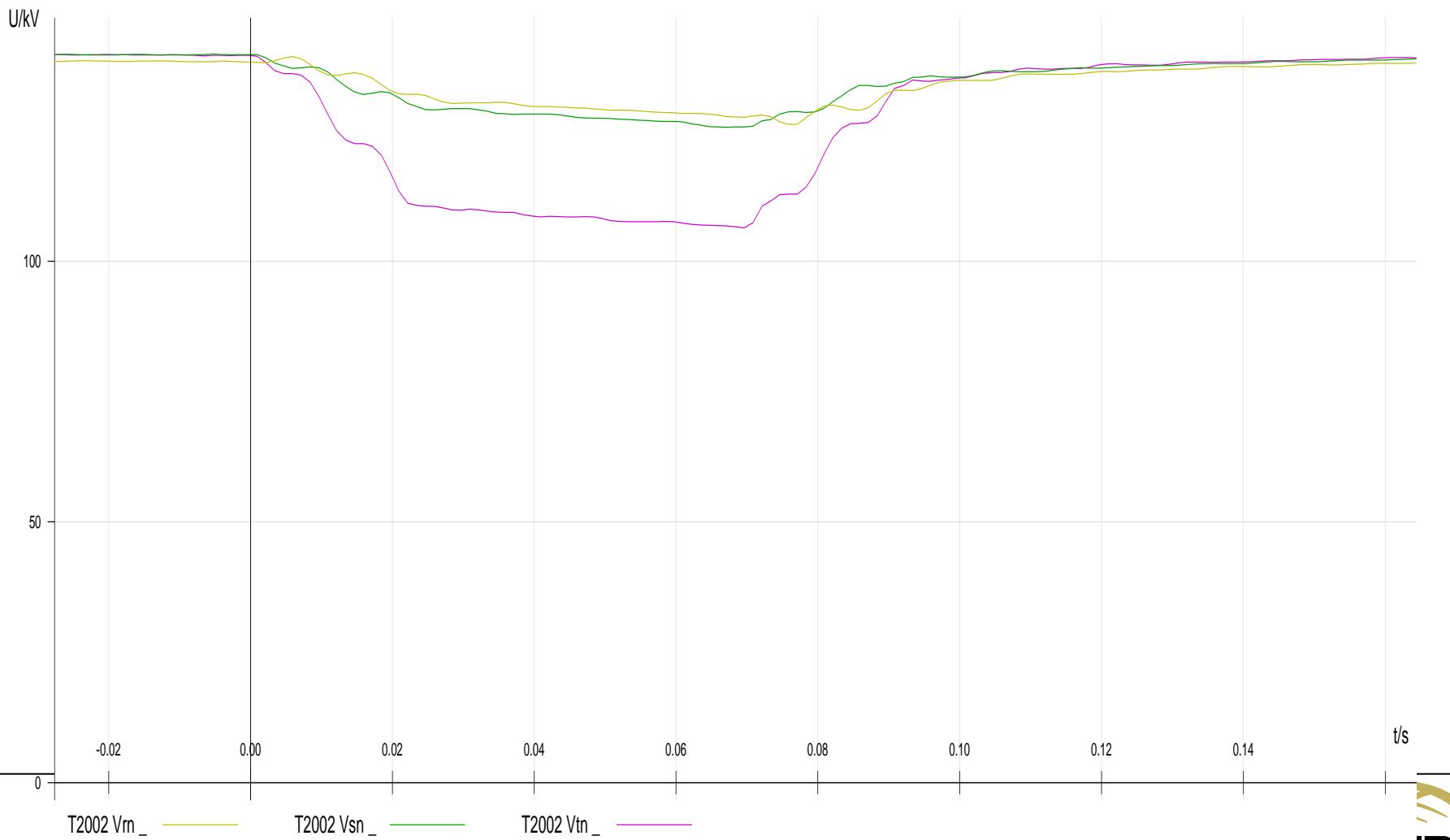
Voltage Dip in Moneypoint 400kV

RMS Voltages R,S,T phases during fault. Taken from T4002 in Moneypoint



Voltage Dip in Longpoint 220kV - Cork

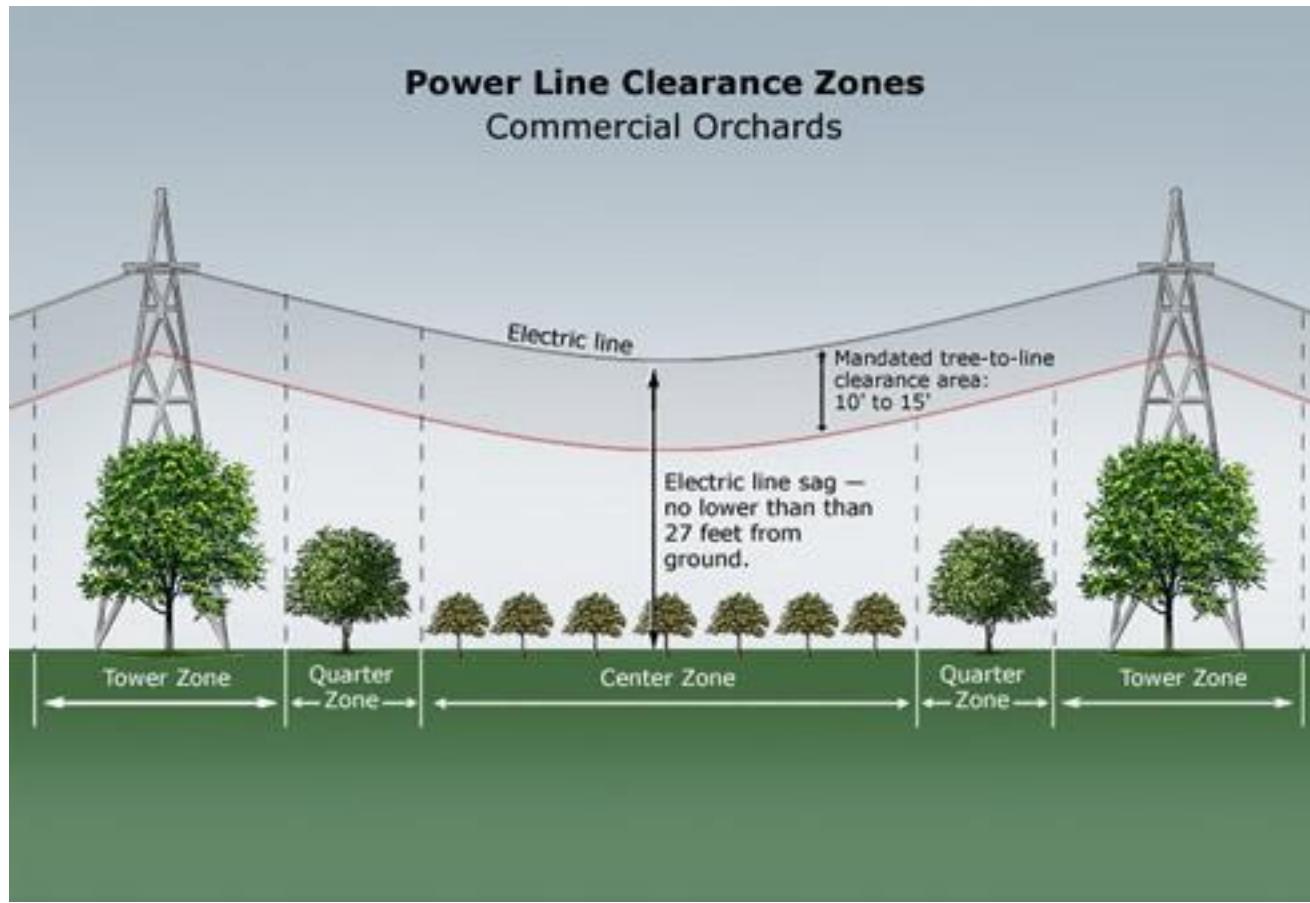
RMS R, S, T Voltages during the fault taken from T2002 in Longpoint



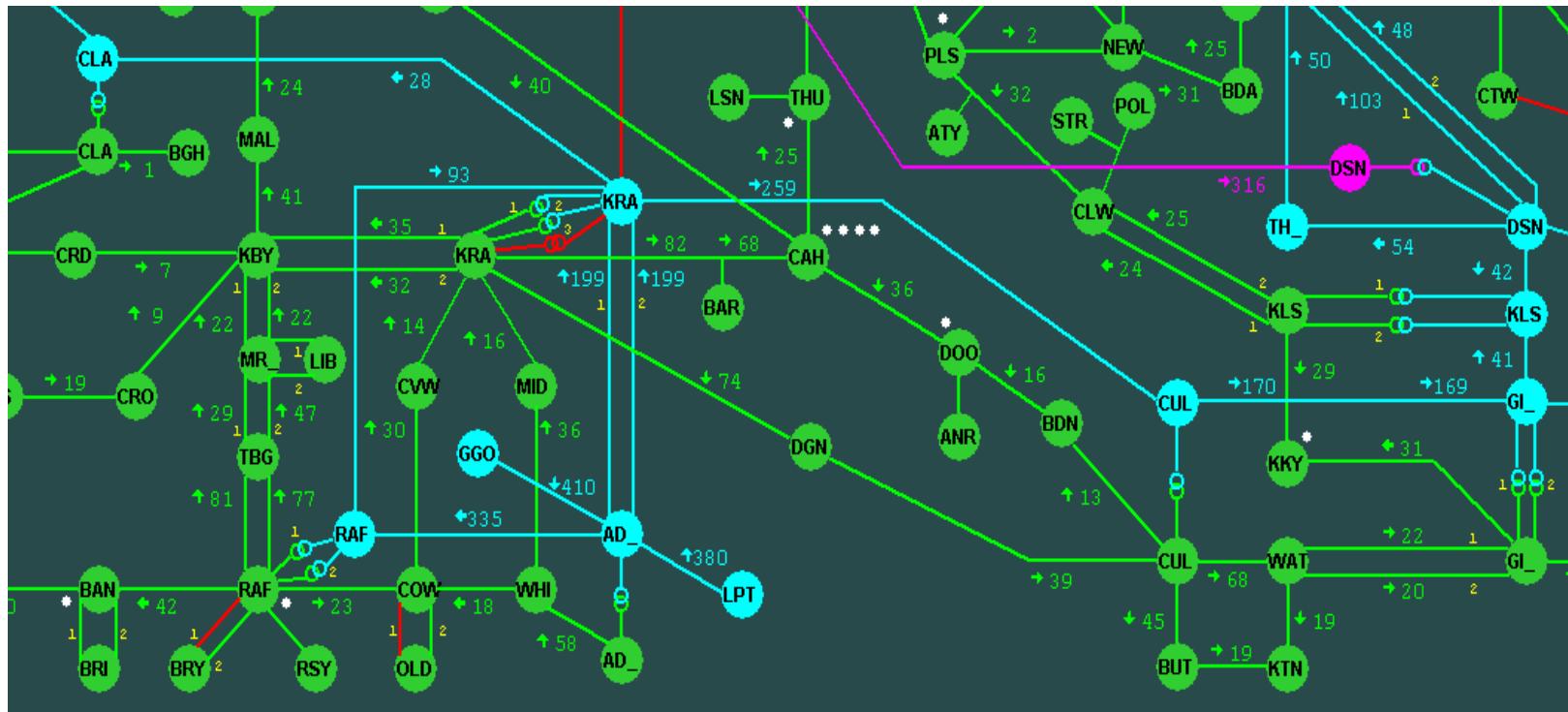
‘System Stats’

• Voltage	No. Stn.	Circuit (km)
• 400kV	4	440
• 220kV	31	1830
• 110kV	159	3850
• 2 x 275kV 600MVA	Tie lines with Northern Ireland	
• 2 x 110kV	Tie lines with Northern Ireland	
• Installed capacity	6,500 MWs	(centrally dispatched)
• Installed Wind	1,469 MWs	
• Power Stations	21	
• Evening Peak	5090 MW	Tues 21/12/2010
• Max Wind	1284 MWs	Sat 12/02/2011
• Wind as % system demand	50%	Mon 5/04/2010





Example Case



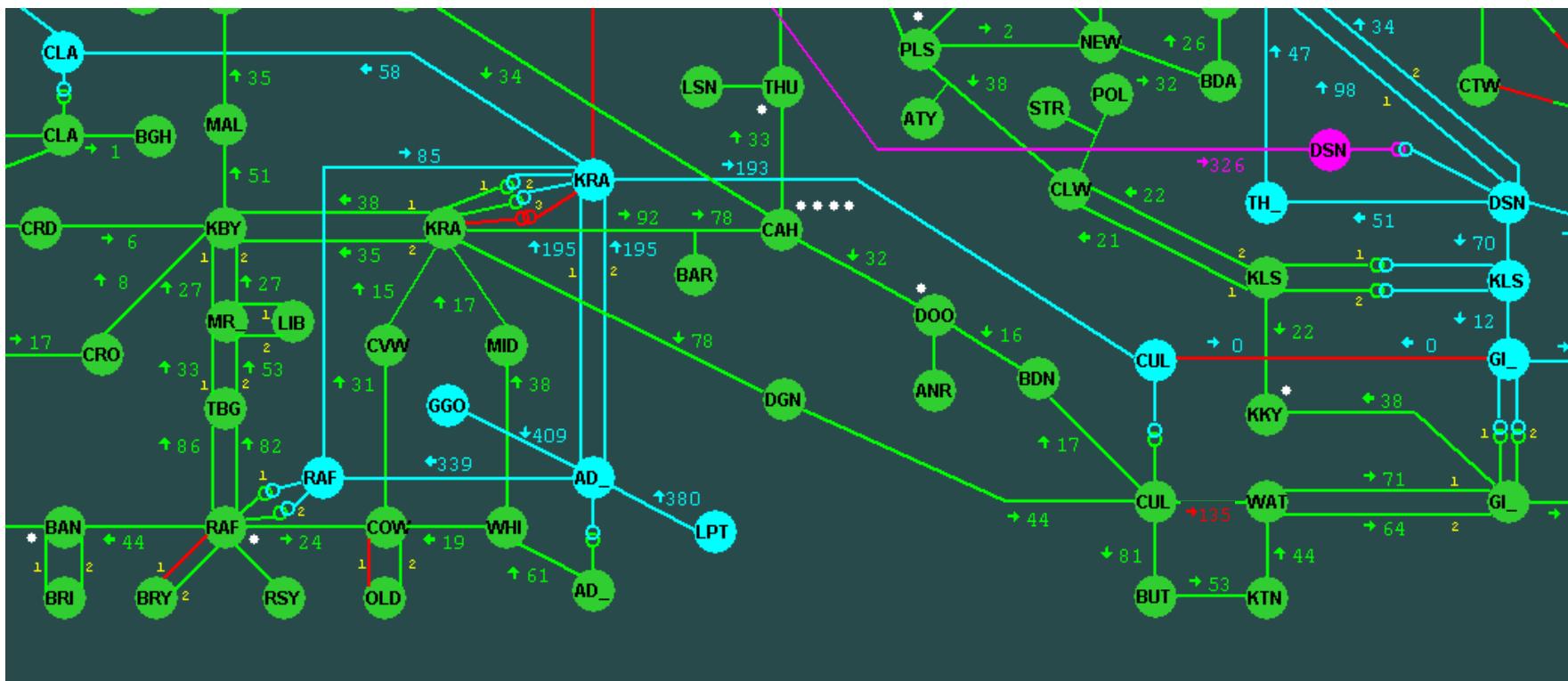
Load 3900 MW

Low wind – 33 MW

Cork Generation – 780 MW

Cullenagh – Waterford 110 kV line (rated 116 MVA)

East - West Contingency



Loss of Cullenagh – Great Island 220 kV line

-> overload on Cullenagh – Waterford 110 kV line

118 % overload on 116 MVA rated line

Power Flow - Why

- Equipment Rating
- Safety
- Secure after n-1

Protection Operations - Tarbert

- In Tarbert: The protection relay detected the fault and issued a 3 pole trip command to the 220 kV circuit breaker on the Prospect line
- The CB opened 69 ms after fault inception. This cleared the fault infeed from Tarbert
- Automatic restoration of the feeder is not in service at the Tarbert end